# Ground Penetrating Radar (GPR) and Electromagnetic Induction (EMI) Surveys Mason Family Cemetery Area

## **Gunston Hall Plantation**

David L. Reese, Director

by

and

William F. Hanna, Ph.D Geophysical Consultant Reston, Va. Claude E. Petrone

National Geographic Society, Ret. College Park, Md.

on behalf of

## **Board of Regents**

and

## The National Society of Colonial Dames of America

Contact:

Dave Shonyo, Staff Archaeologist



with assistance provided by John H. Imlay

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#### INTRODUCTION

## Purpose

Geophysical surveys were conducted in June and July 2006 in an area surrounding the brick-walled Mason Family Cemetery at Gunston Hall Plantation, Fairfax County, Virginia. The purpose of these surveys was to estimate using non-invasive techniques the areal extent of unmarked burials that may reside outside of the cemetery walls. These geophysical surveys included ground-penetrating radar (GPR) and electromagnetic induction (EMI), supplemented by a few measurements of vertical magnetic gradiometry and magnetic susceptibility.

#### Earlier work

Earlier geophysical surveys inside of the cemetery walls--about 300 yards southwest of the mansion (also known as "The Hall")-- indicated the probable presence of as many as 22 adult burials, most not spatially associated with the 8 inscribed markers within the walls.

## Known cemetery burials

A bronze plaque attached to the cemetery wall states

This wall was built in 1922 through the concern and generosity of Lillian Seeligson Winterbotham and other Mason descendants.

## Interred here are

George Mason of Gunston Hall, Patriot	1725 - 1792
Ann Eilbeck Mason	1735 - 1773
James and Richard Mason	1772
George Mason V of Lexington	1753-1796
Elizabeth Mary Ann Barnes Hooe Mason Graham	1768 - 1814
John Graham	1806 - 1811
Richard Graham	1814
George Mason VI of Gunston Hall	1786 - 1834
Elizabeth Thomson Mason Mason	1789 - 1821
Eleanor Ann Clifton Patton Mason	1807 - 1867
John McCarty Mason	1817 - 1837
George Mason Ellzey	1837 - 1838
Richard Barnes Patton Mason	1824 - 1847
William Stuart Mason	1795 - 1857
George Mason of Hollin Hall	1797 - 1870
and others in unmarked graves.	

## Inscribed stones

The cemetery currently contains a total of 8 inscribed markers for 10 persons, all in east-west alignment:

- (1) George Mason IV of Gunston Hall [box tomb]
- (2) Ann Mason, wife of George Mason IV [box tomb]
- (3) George Mason V of Lexington
- (4) Elizabeth Mary Ann Barnes [Hooe] [Mason] Graham, wife of George Mason V of Lexington; the stone indicates that beside her lie her sons, John Graham and Richard Graham
- (5) William [Stuart] Mason, son of William Mason and grandson of George Mason IV
- (6) George [William] Mason [of Hollin Hall], son of Thomson Mason and grandson of George Mason IV
- (7) Eleanor Ann Clifton [Patton], wife of George Mason VI
- (8) "L. G.", presumably unidentified. [W.F. Hanna note: This repaired, footstone-size marker is very similar in shape and composition to the gravestones of Elizabeth Mary Ann Barnes Graham (#4 above) who was the daughter of Gerard and Sarah Hooe of Barnesfield. This "L. G." might correspond to a Graham not known in genealogical records—perhaps an infant. Alternatively, it is of passing interest, because of several coincidences of names, that a descendant of George Mason IV, Lucy Grymes, who died in Barnesfield, married a Hooe, and provided each of her three Hooe children the middle name Barnes. Although Lucy was interred in St. Paul's Episcopal Cemetery, it might be that this gravestone somehow commemorates her name—perhaps having been "saved" and placed within the family cemetery. These are mere speculations.]

In corroboration with some of the information on the bronze plaque, written accounts indicate that others buried in the Mason Family Cemetery, include:

- Richard and James Mason (both d.1772, one day old), twin sons of George Mason IV and Ann Eilbeck
- John (d. 1811, 6 years old) and Richard (d. 1814, an infant) Graham, sons of George Graham and Elizabeth Mary Ann Barnes (widow of George Mason V)—both claimed on an inscribed slab to "lie beside her".
- John McCarty Mason (d. 1837, 20 years old), son of George Mason VI and first wife Elizabeth Thomson Mason
- Richard Barnes Patten Mason (d. 1847, 23 years old), son of George Mason VI and second wife Eleanor Ann Clifton

Our earlier GPR work indicates that gravestones within the walled cemetery do not accurately reflect the exact locations of interments, including the marble box tombs commemorating George Mason IV and his first wife Ann.

We see from J. Harry Shannon's 1905 glass-negative image "Jefferson Walnut Tree at Gunston Hall" that, as noted by authors Connie Pendleton Stuntz and Mayo Sturdevant Stuntz, "not far from the black walnut tree is a grave marked by a simple granite headstone inscribed 'George

Mason, Author of the Bill of Rights and the First Constitution of Virginia 1725-1792'." We also learn from Bertha Louisa Robinson's 1910 article "Pilgrimages to American Landmarks—Gunston Hall" (Journal of American History) that the grave of George Mason IV "is unmarked, but tradition tells us that his body was interred beside that of his wife." In more recent times, the cemetery has gone through the cyclic process of becoming overgrown and then cleared, like many—if not most—others of its age in this part of the country. We have discovered through our work in very old cemeteries elsewhere in northern Virginia that, over time, gravestones have been inadvertently (or sometimes intentionally) moved, broken, repaired, replaced, removed, or naturally buried for any number of reasons, including planned reinterments, accidents during caretaking, vandalism, passive neglect, plowing, and the natural forces of frost-heaving followed by settling. Just as some burials exist in an unmarked state, some gravestones remain in place where no burials exist—notably where re-interments have occurred and where inscribed stones have been purposely "saved" from anticipated destruction and re-emplaced at another burying ground.

The cemetery has long been known as the "Gunston Hall Graveyard" in some records. It is coded as Fairfax County Cemetery #FX144 in the compilation of Brian Conley (1994) and titled by him the "Mason Family Cemetery". The brick wall enclosing it is 50 ft north-south by 40 ft east-west; the bronze plaque indicates that it was constructed in 1922. This wall orientation is congruent with the grave-marker orientation within it—that is, the traditional Judeo-Christian burial pattern of the decedent resting in a supine position oriented west to east with the head to the west.

## Geophysical survey dates, 2006

Following a preliminary meeting of Hanna and Petrone with Dave Shonyo, Staff Archaeologist, at Gunston Hall on June 6, Hanna, Petrone, and Imlay conducted GPR surveys south of the walled cemetery on June 9; west of the cemetery on June 16; east of the cemetery on June 20; and north of the cemetery on June 29. EMI surveys were conducted by Hanna on June 30 and July 6, 7, and 8. A limited amount of probing, soil coring, and troweling was conducted by Imlay and Shonyo on July 7. Hanna and Shonyo observed some vertical magnetic gradiometry and magnetic susceptibility measurements on July 8.

#### Gunston Hall occupancy

Gunston Hall's original owner, George Mason IV (1725-1792), has been described as one of the least known and most influential of America's Founding Founders. Among his many Colonial and Revolutionary accomplishments, he wrote Virginia's Declaration of Rights and its Constitution, both of which influenced Thomas Jefferson's composition of the Declaration of Independence. Gunston Hall was occupied almost continuously by many owners throughout a period of nearly 250 years; one owner in 1875 constructed a cupola atop the mansion to house his telescope. Today, Gunston Hall is a 550-acre National Historic Landmark owned by the

Commonwealth of Virginia and administered by a Board of Regents appointed from The National Society of The Colonial Dames of America.

The "numbered George Mason" line of ascent is as follows:

George Mason VI was the son of George Mason V and wife Elizabeth Mary Ann Barnes Hooe George Mason V was the son of George Mason IV and his first of two wives, Ann Eilbeck George Mason IV was the son of George Mason III and his wife Ann Thomson George Mason III was the son of George Mason II and his first of three wives, Mary Fowke George Mason II was the son of George Mason I and his first of two wives, Mary French

Children of George Mason IV and Ann Eilbeck were George Mason V; Ann Eilbeck Mason; William Mason, died at one year of age; a second William Mason, born one year later; Thomson Mason; Sarah Eilbeck Mason; Mary Thomson Mason; John Mason; Elizabeth Mason; Thomas Mason; and twins Richard Mason and James Mason, who were born prematurely and died one day old. Ann Eilbeck died 3 months after the birth and death of these twins.

## Geographic Setting

Gunston Hall Plantation is located in Fairfax County, Virginia (figure 1), about 14 miles south of Alexandria, on a cove of the Potomac River at geographic coordinates 38.6641° N, 77.1603° W, and elevation 123 ft (GPS and Fort Belvoir 7.5-minute USGS topographic quadrangle). Gunston Hall was constructed mainly during the period 1755-1759 with a probable permanent occupation no later than 1760. Contemporary plantations on or near the Potomac River included Mount Vernon and Marshall Hall to the northeast and Rippon Lodge to the southwest. Gunston Hall has a mailing address of 10709 Gunston Road, Mason Neck, VA 22079 and a worldwide web site of "gunstonhall.org". It is accessed from the Richmond Highway (U.S. Route #1) by traveling about 3.6 miles southeast along Gunston Road (Route 242) and turning left onto the well-marked entrance road. The cemetery survey area is about 300 yards from Gunston Hall, the mansion (figure 2).

## Geologic Setting

Gunston Hall Plantation is situated on the Atlantic Coastal Plain physiographic province. It is underlain by unconsolidated sediments of the Potomac Formation, Cenozoic upland gravels, and Quaternary alluvium. The Potomac Formation consists of medium to coarse sands, silty sands, silty clays, and gravelly sands. The soil surrounding the mansion, including our southwest side-yard survey area, has been labeled "manmade" on a soils map; this term indicates that the soil here is largely introduced fill. The coarse, brown soil at the family cemetery, which has a fragipan at about 2 ft depth, is labeled "Beltsville loam, undulating phase" and has developed from Coastal Plain sand, silt, and clay. Soils topographically higher than the mansion typically consist of a mantle of silty and sandy materials over older river terrace deposits that overlie sedimentary beds of the Potomac Formation. Soils topographically lower than the mansion

typically consist of alternating strata of sands, silts, and clays with some river-deposited cobbles and boulders. The presence of clay is relevant to our GPR surveys in that significant quantities tend to attenuate the signal and thus impede the passage of radar energy into the subsurface.

## Acknowledgments

Staff archaeologist Dave Shonyo and archaeology volunteers—most notably Gretchen Wendelin and Art Eaton--observed the GPR surveys and helped with measurement tapes. Shonyo also participated in the limited amount of probing, coring, and troweling. Staff librarian Kevin Shupe also visited our field site.

Among our GPR team, Pete Petrone, owner and operator of the GPR system, monitored signals received during the surveys, used his custom-made pole-cam digital camera to supply overhead photographs. John Imlay announced the GPR line numbers and distances for audio/video recording, managed antenna cables, and tested soil conditions at a few locations using a steel probe and coring tool. Bill Hanna pulled and timed the antenna passage and analyzed and interpreted the GPR data. Hanna also conducted the EMI surveys, analyzed and interpreted the data, and composed this multi-disciplinary report.

#### EXACTLY WHAT PHYSICAL PROPERTIES WERE REMOTELY SENSED?

Subsurface objects, structural features, or disturbed soil of possible archaeological interest can be remotely sensed by several geophysical techniques. Those most frequently used are GPR, EMI (or, alternatively, galvanic resistivity), and magnetic methods. Each technique senses a different property or combination of properties of a material *if and only if the property appears as a sufficiently strong contrast to that of surrounding material*. The properties sensed in our surveys include induced and remanent magnetization, electrical conductivity, dielectric permittivity, and magnetic viscosity. We have used two primary instruments and two secondary instruments. The primary tools were the GPR system and an EMI instrument used in the in-phase mode. The secondary tools were a fluxgate magnetic locator and a handheld magnetic susceptibility meter. The GPR system mainly sensed dielectric permittivity or electrical conductivity. The EMI instrument sensed magnetic susceptibility of soil or anti-phased high electrical conductivity of metal, or both, in its in-phase mode. The secondary instruments measured induced and remanent magnetization of soil, brick and other materials.

#### GROUND-PENETRATING RADAR SURVEY

#### Instrumentation

GPR measurements were made by using a Subsurface Interface Radar system SIR-8, manufactured by Geophysical Survey Systems (GSSI), Inc. (figure 3). The antenna used with this system acts both as the transmitter and receiver of radar energy—this is called operating in

"monostatic mode". The principle of operation is that pulses of multi-frequency energy are transmitted into the subsurface by the antenna which is pulled continuously along the ground surface. Where the transmitted energy encounters an interface of contrasting electromagnetic properties--an object or other feature--, some of the energy reflected (or back-scattered) from the interface will be received by the antenna. By noting the positions of signals on the radar record (or radargram), one can draw inferences about both the horizontal and vertical locations of an object or feature in the subsurface.

By carefully measuring the two-way time between the transmitted and received energy, one can infer the distance between the antenna and reflecting interface *if the average velocity of energy travel in the soil can be reasonably estimated*. It should be emphasized that one of the virtues of the GPR technique over other lower-frequency electromagnetic techniques (such as EMI) is that it is capable of sensing *non-metallic* targets as well as *metallic* targets.

On the basis of previous work, we elected to use an antenna having a central frequency of 500 MHz. This antenna is shielded in order to effectively eliminate any upward generation of signal that might reflect from overhead tree limbs or wires. The antenna is "broadband", meaning that it generates energy in a bandwidth of about 250 MHz to 1 GHz downward in the approximate shape of an elliptical cone. As a result of this conical shape, the antenna "sees" not only downward, but also a certain distance forward and backward as well as to either side. The transmitter generated pulses at a repetition rate of 50,000 times per second; reflections were recorded at a rate of 12.8 scans per second.

In these surveys, the antenna was continuously moved on the ground surface along parallel lines spaced 18 inches apart. The antenna was moved at a time-regulated rate of 50 ft/min. Time marks were inscribed on each GPR record at an interval of 5 ft. Two closely spaced time marks on the resulting record delineate the beginning and end of each line. The scan range (duration of recording of each scan line) was set at 36 nanoseconds (abbreviated "ns"; one ns is one-billionth of a second) on the basis of field tests. Filter settings were retained at low values to maximize the amount of returned signal. All of the data were displayed real-time on a GV-8 color monitor via a Model 38 Video Display Unit manufactured by GSSI, Inc. The color linescans were recorded on the GV-8 in 8-mm video tape format for further analysis.

Each recorded scan represents a wiggly reflected signal (not seen, except through use of post-surveying computer software) that has a variable amplitude greater or less than operator-set color thresholds. Thus, on the video screen, each scan takes the form of a skinny vertical line composed of many colored segments, each color corresponding to signal amplitude or "strength". The top of any scan line represents the start of the scan at the antenna; the bottom of the scan line represents the two-way travel time of the reflected radar energy (time required to travel from "antenna acting as transmitter" - to - "subsurface reflector" - to - "antenna acting as receiver"). The complete color linescan record seen on the video screen is the side-by-side ensemble of all of these skinny multi-color lines. In our records, bright whites, reds, yellows and greens usually

represent large-amplitude positive signals and dark blues usually represent large-amplitude negative signals. Most moderately sized signals are various shades of gray.

The zero time mark and the duration of the near-field zone (where the transmitted signal is coupled to the uppermost part of the subsurface) was subjectively determined by comparison with other records previously acquired by this system under identical parameter settings. Each color linescan record shows (1) from left-to-right, distances at 5-foot intervals in the direction indicated on the radargram and (2) from top-to-bottom, the 2-way travel time (from transmitter-to-reflector-to-receiver) of the reflected signal in nanoseconds (ns), a total of 36 ns (vertical scale).

Our experience suggests that a reasonable estimate of the average velocity of radar energy in this soil is about 1/3 ft per nanosecond. Thus, we expect a reflection observed *halfway down* on the color timescan record (about 18 ns of 2-way travel time) to correspond to a reflector depth of about 3.0 ft; a reflection observed at the bottom of the record (about 36 ns of 2-way travel time) would correspond to a depth of about 6.0 ft. Where the soil velocity varies significantly in a lateral direction, the estimate of depth likewise varies.

## GPR record analysis

After completion of field work, the data were analyzed by viewing and reviewing the video tape records on a Sony Trinitron 25-inch high-resolution NTSC television monitor. A transparent template with 36 major tick increments along its vertical axis was used to pick best estimates of first arrivals of primary reflections.

Ordinarily, the most conspicuous GPR reflections in a given area have the shape of a hyperbola or upward arch. This shape usually results from the reflection of radar energy from a single underground object--ideally a "point source". These signals resemble those of sonic echo-finders used by fishermen. Ideally, a well-formed hyperbolic echo in GPR work results when energy reflects from an object with a circular or curvilinear top, such as a horizontal cylinder (pipe or conduit), sphere, top of a tunnel--or in a graveyard, top of coffin. In practice, hyperbolic echoes are often broken, distorted, asymmetrical, or obscured by interfering signals from nearby objects or by other noise. A given reflector may be a rock, brick, tree root, animal burrow, conduit, utility line, tunnel, ditch, wall foundation, air- or water-filled void, or any metallic, ceramic, glass, or plastic object. Within a graveyard, a reflector may be any feature of a burial container or its contents--such as a knotty portion of a pine box, coffin hardware, a viewing pane, more massive bones, or a ceremonial object buried with the decedent.

A hyperbolic echo on rare occasions can underlie strong secondary reflections from a V-shaped trench ("bowtie" signature); can be produced from the "velocity pullup effect" associated with a large subsurface void--also applicable to some graves; and can be generated from constructive wave interference patterns. Other conspicuous GPR reflections can take the form of horizontal to sub-horizontal bands, corresponding to flat subsurface features (such as a buried root cellar) or

soil facies, or conspicuous columns of reverberations caused by multiple reflections from metallic objects.

## GPR presentation of results

The color linescans are examined and notes are taken on the location, two-way travel time, and relative strength of hyperbolic echoes. For plotting purposes, the hyperbolic echoes are separated into 4 categories: "shallow & weak", "deep & weak", "shallow & strong", and "deep & strong". The break between "shallow" and "deep" is made at the 18 ns two-way travel time mark. Thus, if the average soil velocity is 1/3 ft per ns, "shallow" reflectors are those less than 3 ft deep. Those taken to be "weak" are those of amplitudes 1 and 2; those taken to be "strong" are those of amplitudes 3, 4, and 5. In a cemetery setting, we also commonly note, in a subjective manner based upon our experience, those signals that seemed likely to represent graves. The notes also include some abbreviated descriptive comments.

#### IN-PHASE EMI SURVEYS

The EM measurements were made with a Model EM-38 Conductivity Meter manufactured by Geonics Limited (figure 4). The principle of operation is that, after a small transmitter coil at one end of the elongate instrument generates a magnetic field downward into the soil, this field induces a magnetization in the soil or induces eddy currents within electrically conductive material, or both, that can be detected by a small receiver coil at the opposite end of the instrument. This signal will contain both in-phase and quadrature-phase components, that are respectively "in step" and 90 degrees "out of step" with respect to the transmitting signal. This device operates at a frequency of 14.6 kHz (much lower than frequencies used in GPR) and was designed to detect magnetic susceptibility to a depth of about 2 ft or metallic conductivity to a depth of about 4 ft. Measurements were made in walking mode at a 12-inch station interval along lines spaced 18 inches apart. At each field location, measurements were made on the ground surface with the long axis of the instrument parallel to the traverse line. All of the data were recorded real-time on a data logger--the Omnidata 720 Polycorder. The Polycorder data were later downloaded to a computer for processing, analysis, and display.

It is conventional to express in-phase results when using the Polycorder in units of "ppt"--that is, parts-per-thousand of the ratio of in-phase secondary field to in-phase primary field. However, for archaeological purposes, the in-phase and quadrature-phase units can be simply and conveniently expressed as "IP units".

#### COORDINATE SYSTEM

We used the same coordinate system that we established for our 2005 work (Hanna and Petrone, 2005). In each region surrounding the cemetery, our measurement tapes were aligned north-south, parallel to the long dimension of the brick wall. The coordinate origin was retained near

the southwest corner, inside of the cemetery wall-approximately 3 ft east of the outside edge of the west wall and 6 ft north of the outside edge of the south wall.

We set up measurement tapes 3 ft apart and pulled the GPR antenna (which is 1-ft wide) along 2 lines within each lane formed by 2 adjacent tapes. Thus, the edge of the antenna along each of these 2 lines was 3 inches from the closest tape. This procedure ensures that the tapes are not disrupted by dragging while the antenna is moved. For EMI work, it was convenient to carry the instrument directly (and slightly) above each tape and then along a line halfway between adjacent tapes. Thus, both the GPR and EMI data were acquired at an 18-inch spacing but the two data sets are offset slightly from each other. This offset is shown in **figure 5** which indicates the map locations of GPR lines and EMI measurement points. The brown lines south of the cemetery represent GPR lines 1 - 74, run north to south; red, blue, and green lines west, east, and north of the cemetery represent GPR lines 75 - 103, 104 - 137, and 138 - 165, all run south to north. As noted above, these sets of GPR lines were run on 4 separate field days; the EMI subsets of data were acquired on other days.

Measurement tapes laid out west and east of the cemetery are shown in photographs of **figure 6**. Tapes laid out north of the cemetery are shown in the top photograph of **figure 7**.

#### **RESULTS**

## Preliminary analysis of GPR echoes

For a very preliminary analysis, all GPR echoes (regardless of signal strength and depth-to-reflector) were plotted in relation to the cemetery wall (figure 8). Also plotted were highly subjective inferences about characteristics of some of these echoes—whether "grave-like", "tree root-like", or "classic" in some significant sense (e.g., exceptionally well formed and thus a textbook example). This map was merely a working tool to be used also in conjunction with EMI data. South of the cemetery, 89 echoes were in some sense "grave-like", 17 were "root-like", and 12 were "classic" or especially significant. West of the cemetery, 51 echoes were in some sense "grave-like", 103 were "root-like", and 8 were "classic" or especially significant. East of the cemetery, 19 echoes were in some sense "grave-like", 213 were "root-like", and 24 were "classic" or especially significant. North of the cemetery, 38 echoes were in some sense "grave-like", 83 were "root-like", and 8 were "classic" or especially significant.

In the more highly developed maps that follow, "deep" refers to a depth-to-reflector of 2 ft or greater, assuming a radar velocity in soil of 1/3 ft per nanosecond.

## Area south of cemetery

GPR echoes and lateral discontinuities along the 74 lines south of the cemetery are shown in **figure 9**. Also shown are regions of significant in-phase EMI anomalies, as displayed in more detail in **figure 10**, representing 1,804 measurement points.

Among the 451 echoes noted (**Appendix A**), 93 ( $\sim$  20 %) are "shallow & weak", 233 ( $\sim$  52 %) are "deep & weak", 113 ( $\sim$  25 %) are "shallow & strong", and 12 ( $\sim$  3 %) are "deep & strong". Echo alignments, together with other observations, suggest the likelihood of 15 graves and evidence suggestive of 13 others. Many, if not most of these echoes, also may be associated with invading tree roots. Examples of GPR echoes are shown in **figure 11.** 

The EMI map shows a distinctive east-west string of bubble anomalies at northing coordinate -18 ft (that is, 18 ft south of the coordinate base line or about 12 ft south of the outside south wall of the cemetery). This string may mark a former fence line. The large isolated bubble anomaly at coordinate (-13.5', -2') has not been investigated but it appears near where an east-west alignment of GPR echoes was detected.

## Area west of cemetery

GPR echoes and lateral discontinuities along the 28 lines west of the cemetery are shown in **figure 12**. Also shown are regions of significant in-phase EMI anomalies, as displayed in more detail in **figure 13**, representing 434 measurement points (an additional 1,085 in-phase EMI measurements were made in this area in 2005).

Among the 405 echoes noted (**Appendix A**),  $122 (\sim 30 \%)$  are "shallow & weak",  $165 (\sim 41 \%)$  are "deep & weak",  $107 (\sim 26 \%)$  are "shallow & strong", and  $11 (\sim 3 \%)$  are "deep & strong". Echo alignments, together with other observations, suggest the likelihood of 3 graves and evidence suggestive of 21 others. Many, if not most of these echoes, also may be associated with invading tree roots. Examples of GPR echoes are shown in **figure 14**.

The EMI map shows an east-west string of bubble anomalies at northing coordinate +38 ft extending across the small area surveyed from easting -47 ft to easting -28 ft. This string may mark part of a fence line. The single isolated anomaly at coordinate (-36', +60') has not been investigated.

#### Area east of cemetery

GPR echoes and lateral discontinuities along the 33 lines east of the cemetery are shown in **figure 15**. Also shown are regions of significant in-phase EMI anomalies, as displayed in more detail in **figure 16**, representing 1,234, 647, 160 measurement points, respectively, in the main eastern region (upper left), east wall region (upper right), and far east region (lower right).

Among the 420 echoes noted (**Appendix A**), 97 ( $\sim$  23 %) are "shallow & weak", 117 ( $\sim$  28 %) are "deep & weak", 196 ( $\sim$  47 %) are "shallow & strong", and 10 ( $\sim$  2 %) are "deep & strong". Echo alignments, together with other observations, suggest the likelihood of 4 graves and evidence suggestive of 22 others. Many, if not most of these echoes, also may be associated with invading tree roots. Examples of GPR echoes are shown in **figure 17**.

The EMI map shows 3 prominent anomalies and one string segment of bubble anomalies. One prominent anomaly is associated with the iron gate post and gate of the brick-walled cemetery. Another prominent anomaly at coordinate (+79', +9') was investigated with a fluxgate gradiometer and troweled by Dave Shonyo. This anomaly is caused at least in part by shallowly buried barb wire. The third prominent anomaly at the northeast corner of the brick wall was probed and cored by John Imlay, as discussed below. The string of bubble anomalies was detected in the detailed survey and occurs at a northing coordinate of +3 ft. it extends at least from easting 76 ft to easting 87 ft, possibly representing part of a fence line.

## Area north of cemetery

GPR echoes and lateral discontinuities along the 27 lines south of the cemetery are shown in **figure 18**. Also shown are regions of significant in-phase EMI anomalies, as displayed in more detail in **figure 19**, representing 1,396 measurement points.

Among the 245 echoes noted (**Appendix A**), 38 ( $\sim$  16 %) are "shallow & weak", 82 ( $\sim$  34 %) are "deep & weak", 102 ( $\sim$  41 %) are "shallow & strong", and 23 ( $\sim$  9 %) are "deep & strong". Echo alignments, together with other observations, suggest the likelihood of 7 graves and evidence suggestive of 3 others. Many, if not most of these echoes, also may be associated with invading tree roots. Examples of GPR echoes are shown in **figure 20**.

The EMI map shows one prominent anomaly immediately outside at the northeast corner of the cemetery and one moderate anomaly at coordinate (0', +65'), the latter of which has not been carefully investigated. The prominent anomaly was inspected with a fluxgate gradiometer and troweled by Dave Shonyo. It is caused at least in part by shallowly buried spiral fencing wire.

Results of probing/coring based on EMI data....buried arched vault?

A limited amount of probing and soil coring was conducted by John Imlay and Dave Shonyo at one site inside of the walled cemetery and at another site immediately outside of the cemetery at its northeast corner. This probing and coring was requested by Hanna because of observations he made using in-phase EMI data. While analyzing the EMI anomaly at the northeast corner (which unfortunately seems to extend beneath the brick wall which precludes it from being mapped completely), Hanna observed that the gradient (closeness of contour lines) and plan-view size of the feature may be comparable to that associated with the inferred "iron coffin" feature inside of the cemetery. This inferred "iron coffin" location is unmarked (no grave stone) but was mapped remotely using GPR, in-phase and quadrature-phase EMI, and vertical magnetic gradiometry (Hanna and Petrone, 2005). In the process of re-analyzing the "iron coffin" anomaly for this study, Hanna constructed a computer model that suggested the burial site is wider than that of a single coffin. This model suggested that the "iron coffin" burial may be a vault, possibly wide enough to accommodate 2 side-by-side coffins. The likelihood that at least one of the coffins is iron remains valid. John Imlay cored this subsurface feature and discovered that it appears to be about 4.5 to 5 ft wide with its central top at a depth of 16 inches, laterally changing to a depth of

23 inches, possibly indicating an arched vault. One core hole at the plan-view center recovered a circular disc-shaped fragment that appears to be mortar.

Coring at the northeast corner EMI anomaly yielded depths to the top of subsurface object of 33 inches, 25 inches 23 inches, and 22.5 inches, the latter ones remarkably similar to the outer-depths at the "iron coffin" site. There remains, therefore, the possibility that the northeast corner feature is a burial feature—possibly a vault.

#### **CONCLUSIONS**

Tree roots pervasively underlie the ground surface surrounding the brick-walled Mason Family Cemetery, including the open grassy areas. Analysis of GPR data suggests the likelihood of 29 adult-sized graves outside of the cemetery wall and many other possible grave sites (figure 21). Some—if not most—of these inferred graves appear to be invaded by tree roots. Children's graves are too small to be located without visual inspection of subsoil, which would require the temporary removal of topsoil.

Alignments of GPR echoes and the presence of strings of EMI bubble anomalies suggest the presence of several east-west features that may mark parts of fence lines or wall foundations. We cannot comment on the possible presence of counterpart north-south features because such inferences would have to derive from surveys oriented perpendicular to the ones we conducted. Metal detecting may help pinpoint such features.

Further analysis of the "iron coffin" feature inside of the cemetery wall, based on new computer modeling, suggests that the burial site is wider than that for a single coffin. This 3-D model suggests that the "iron coffin" burial may be a vault, possibly wide enough to accommodate 2 side-by-side coffins. If true, he likelihood that at least one of the coffins is iron remains valid. Soil coring at this site recovered a fragment of the top of this feature that appears to be mortar.

The GPR and EMI data both suggest the presence of a subsurface burial feature beneath the northeast corner of the brick-walled cemetery. The geophysical anomalies of this subsurface feature appear similar to those associated with the "iron coffin" feature but they unfortunately cannot be completely mapped because of the presence of the brick wall.

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- Shonyo, David, 2006, Gunston Hall to undertake additional investigations in cemetery area: The Datum Point [Newsletter of the Northern Virginia chapter of the Archeological Society of Virginia], May, 2006, p. 5.

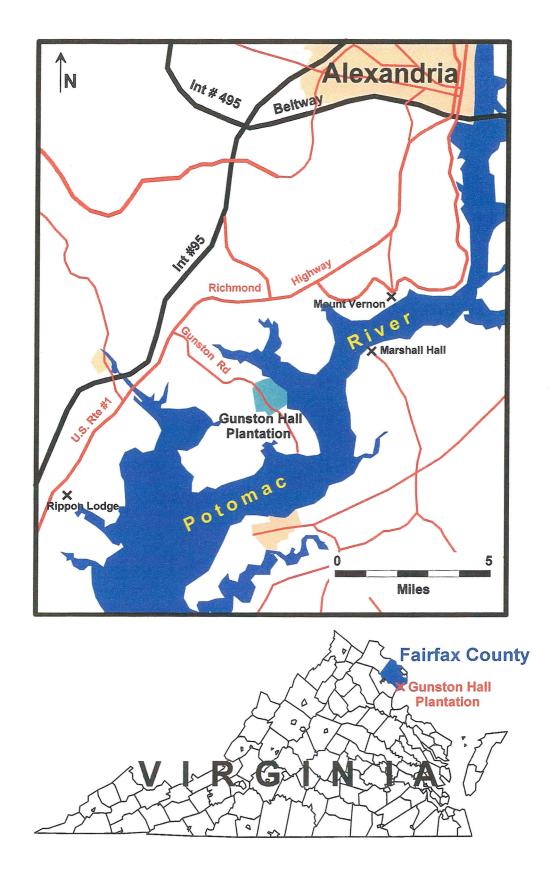


Figure 1. Regional map showing Gunston Hall Plantation.

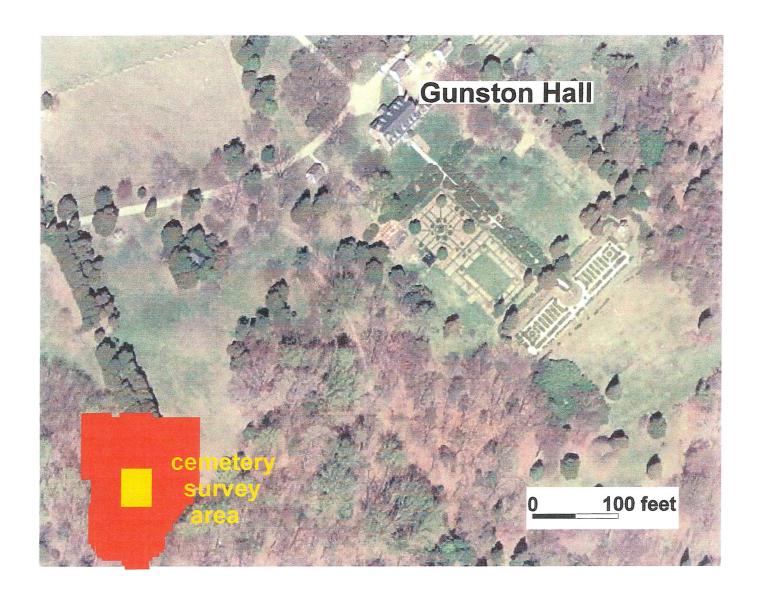


Figure 2. Aerial photograph showing the cemetery (yellow), surveyed in 2005, and surrounding geophysical survey area (red) in relation to Gunston Hall.

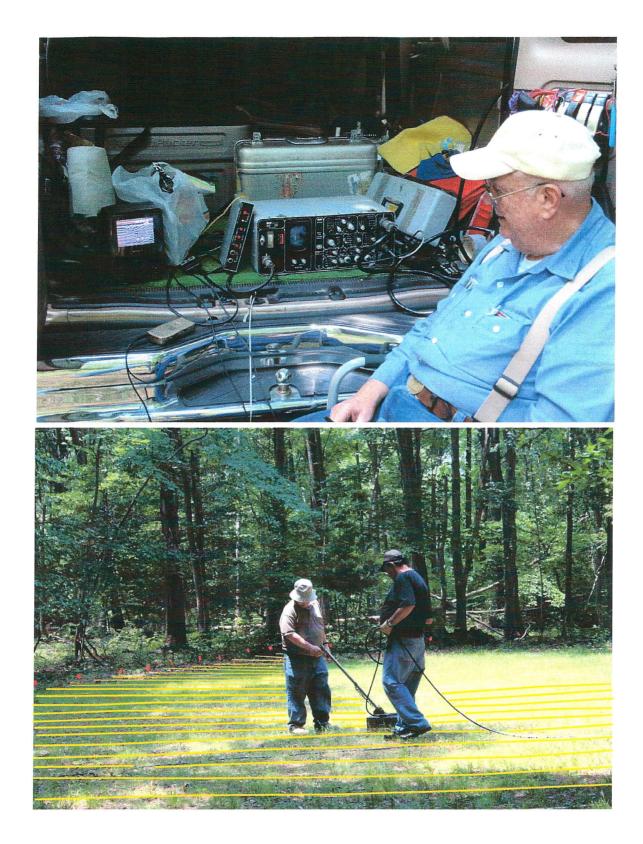


Figure 3. Top: Claude E. "Pete" Petrone operates the electronic equipment associated with the GPR system. Bottom: Bill Hanna (left) and John Imlay operate the 500-MHz antenna south of the walled cemetery.

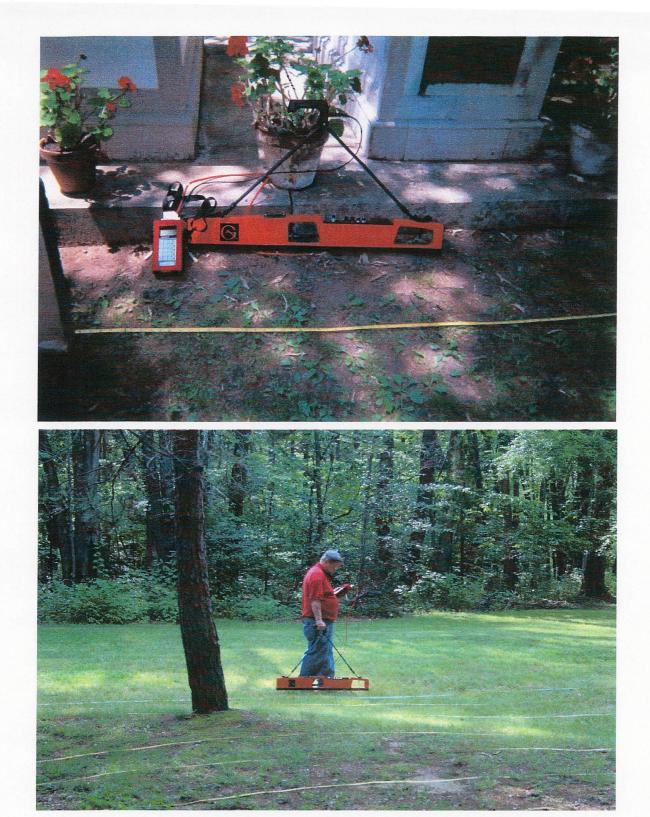


Figure 4. Top: Geonics EM-38 conductivity meter (orange) with attached microprocessor-based polycorder (red). Bottom: EMI survey in progress north of the cemetery.

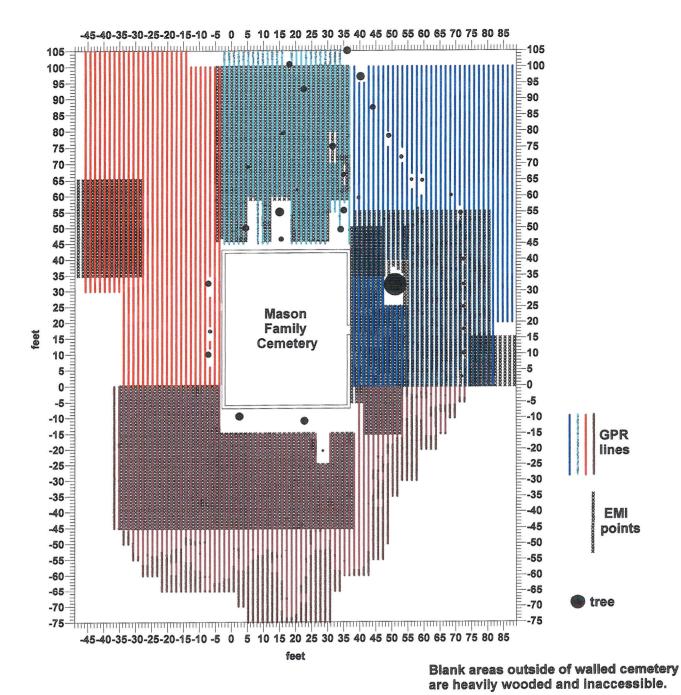


Figure 5. Locations of GPR lines and EMI measurement points.



Figure 6. Top: Measurement tapes west of cemetery. Bottom: Measurement tapes east of cemetery. The large Spanish Oak [Southern Red Oak] tree in the bottom photograph is now more than 200 years old, as determined by dendrochronology.

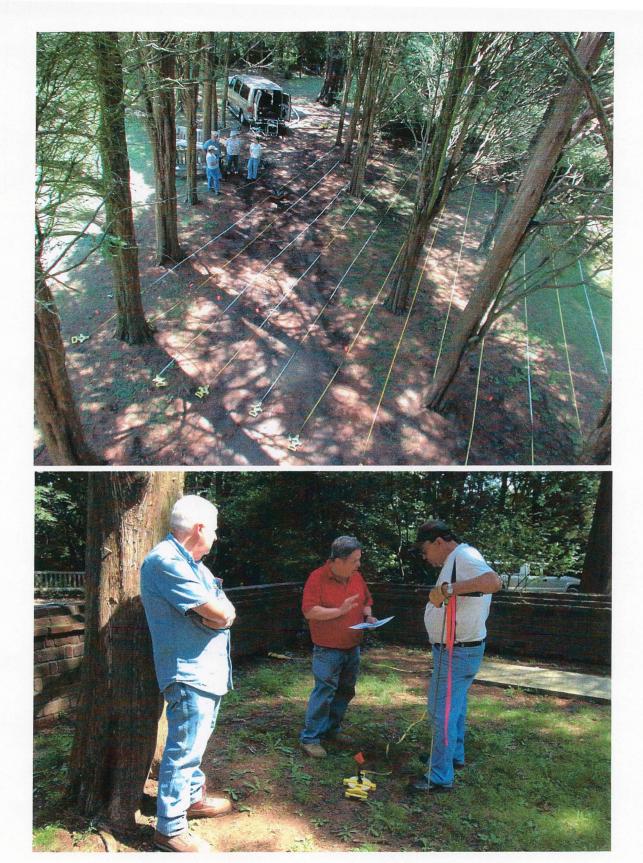


Figure 7. Top: Measurement tapes north of the cemetery, looking south. The tapes diagonally cross a pathway bordered by two rows of cedar trees. Archaeology volunteers gathered near Petrone's van will observe the GPR data collection. Bottom: Dave Shonyo (left), Staff Archaeologist, looks on as Hanna and Imlay record probing and coring data.

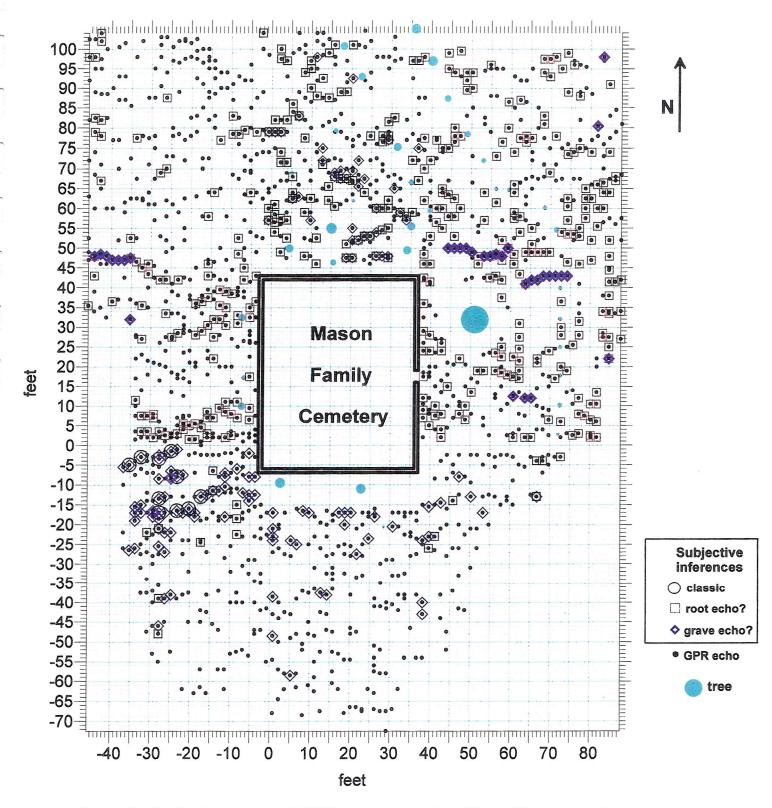


Figure 8. Preliminary map of GPR echoes, unclassified with respect to signal strength and depth-to-reflector, with symbol notations for subjective inferences of tree roots, graves, and video-worthy capture ("classic") for display.

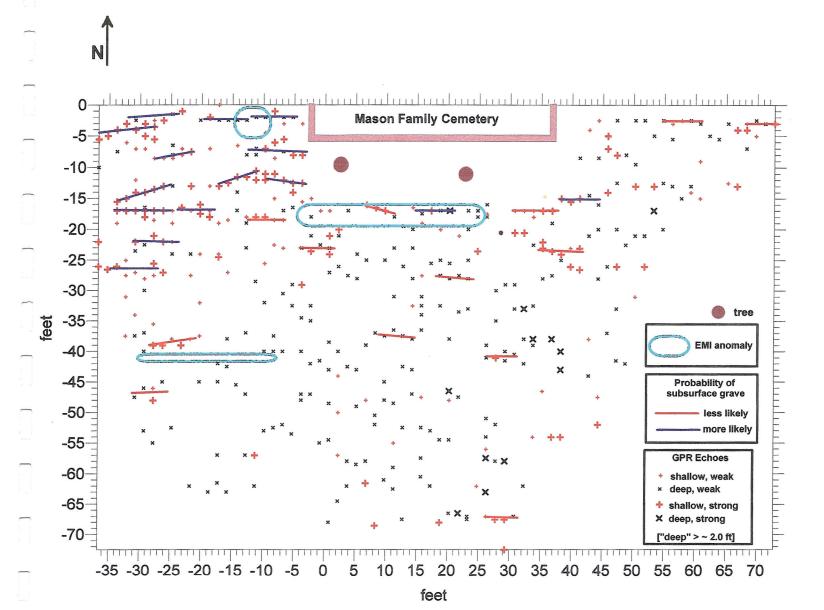


Figure 9. GPR echoes (classified by signal strength and depth) and regions of major EMI anomalies south of the brick-walled cemetery. Echo alignments, which were determined in part by subjective inferences of root-like and grave-like radar signatures, refer to the probability of a grave occurrence. The southernmost linear region of EMI anomalies is based on 2005 data.



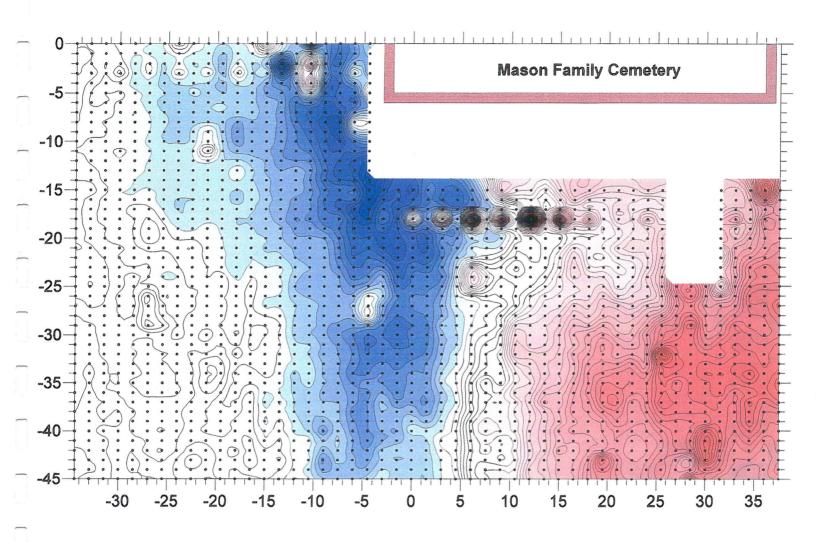


Figure 10. In-phase EMI anomalies over part of the GPR-surveyed area south of the cemetery.

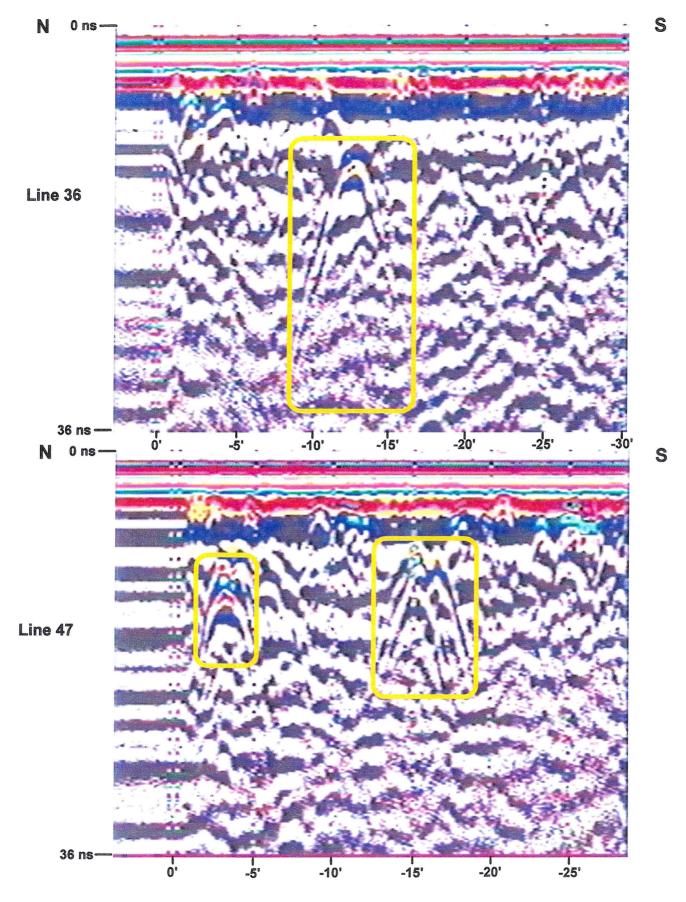


Figure 11. GPR record segments for Line 36 (upper) and Line 47 (lower) south of the walled cemetery, showing major echoes suggesting graves, possibly invaded by tree roots.

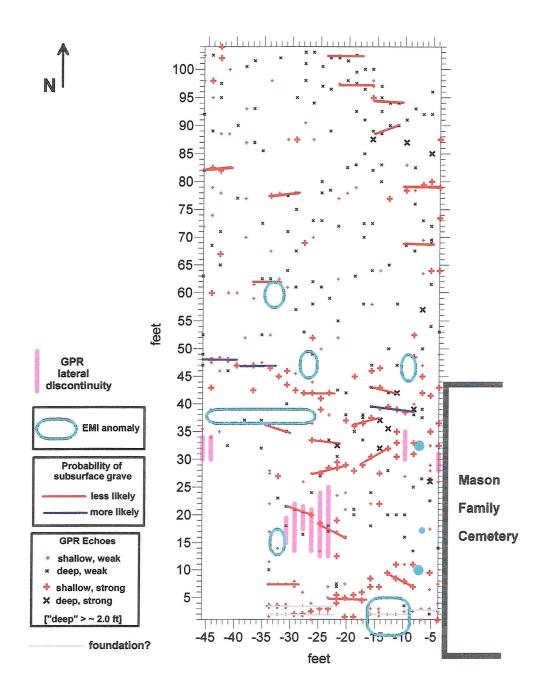
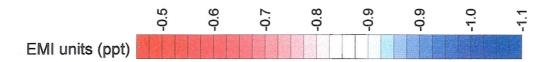


Figure 12. GPR echoes (classified by signal strength and depth), GPR lateral discontinuities, and regions of major EMI anomalies west and northwest of the brick-walled cemetery. Echo alignments, which were determined in part by subjective inferences of root-like and grave-like radar signatures, refer to the probability of a grave occurrence.



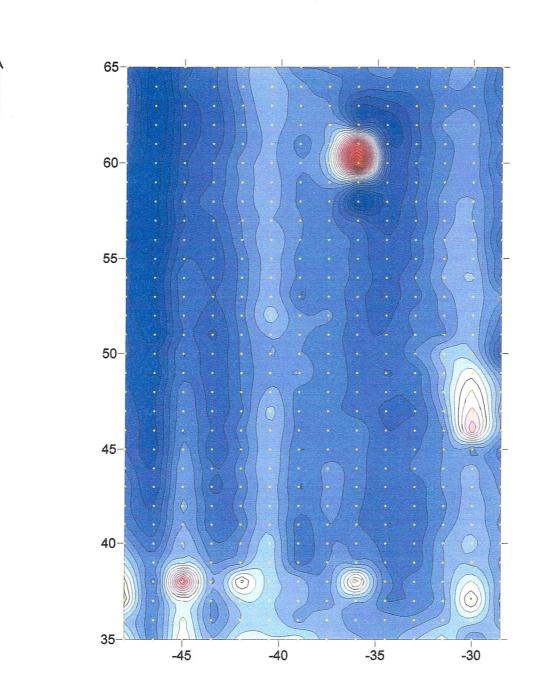


Figure 13. In-phase EMI anomalies over part of the GPR-surveyed area west of the cemetery.

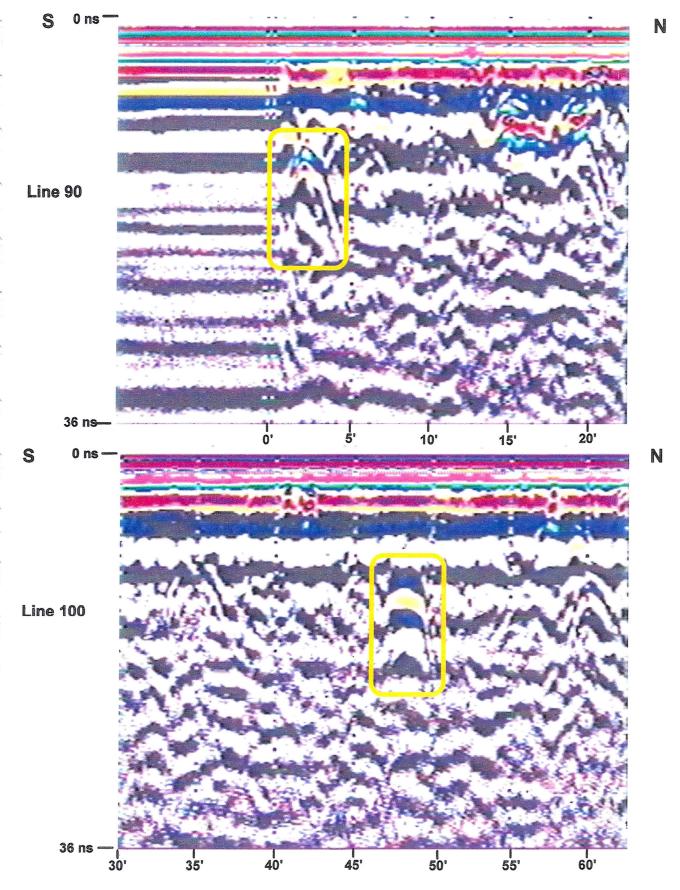


Figure 14. GPR record segments for Line 90 (upper) and Line 100 (lower) west of the walled cemetery, showing major echoes suggesting a foundation (Line 90) and a grave with metallic content (Line 100).

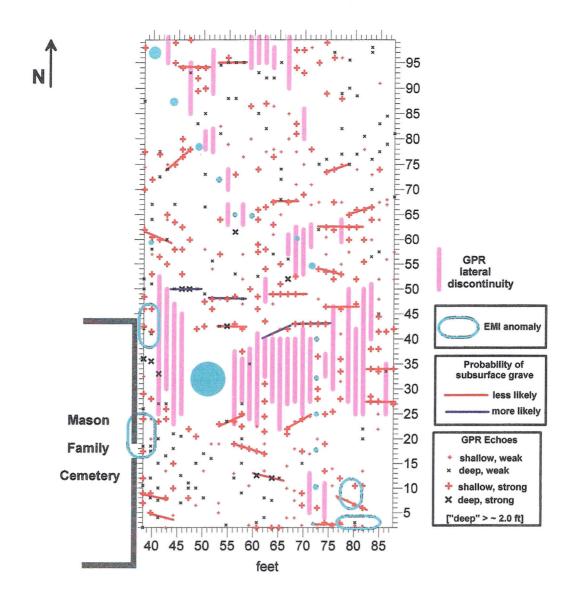
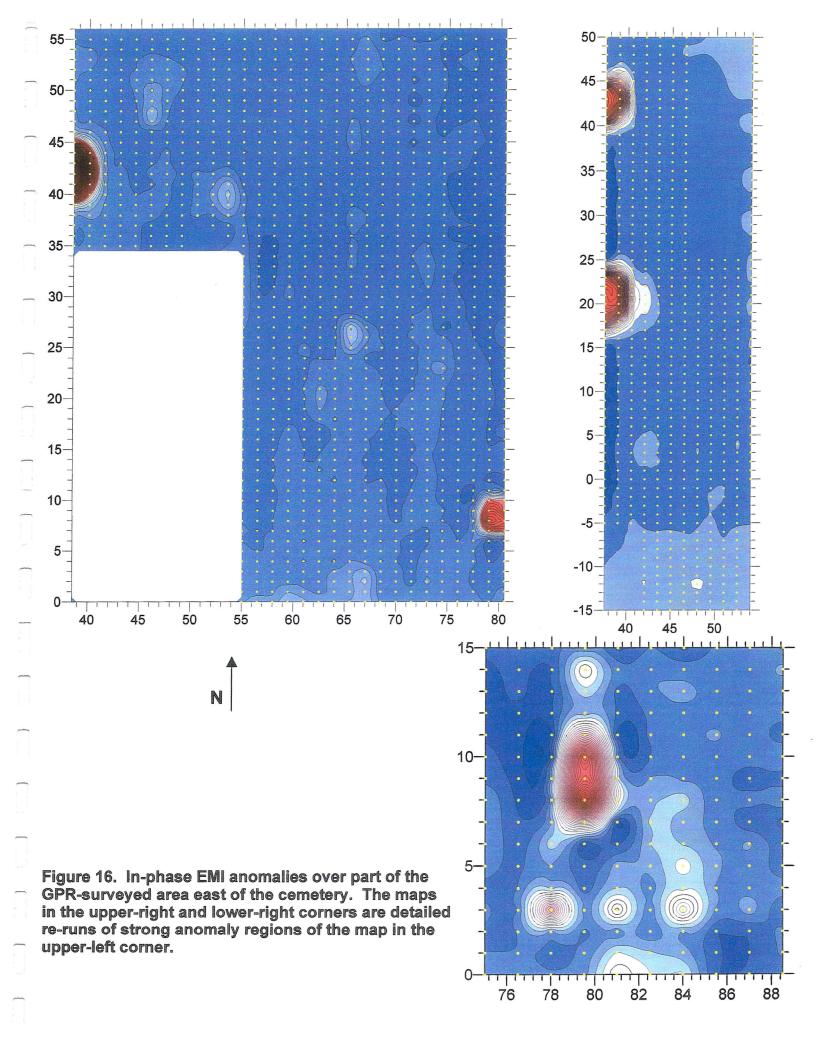


Figure 15. GPR echoes (classified by signal strength and depth), GPR lateral discontinuities, and regions of major EMI anomalies east and northeast of the brick-walled cemetery. Echo alignments, which were determined in part by subjective inferences of root-like and grave-like radar signatures, refer to the probability of a grave occurrence.



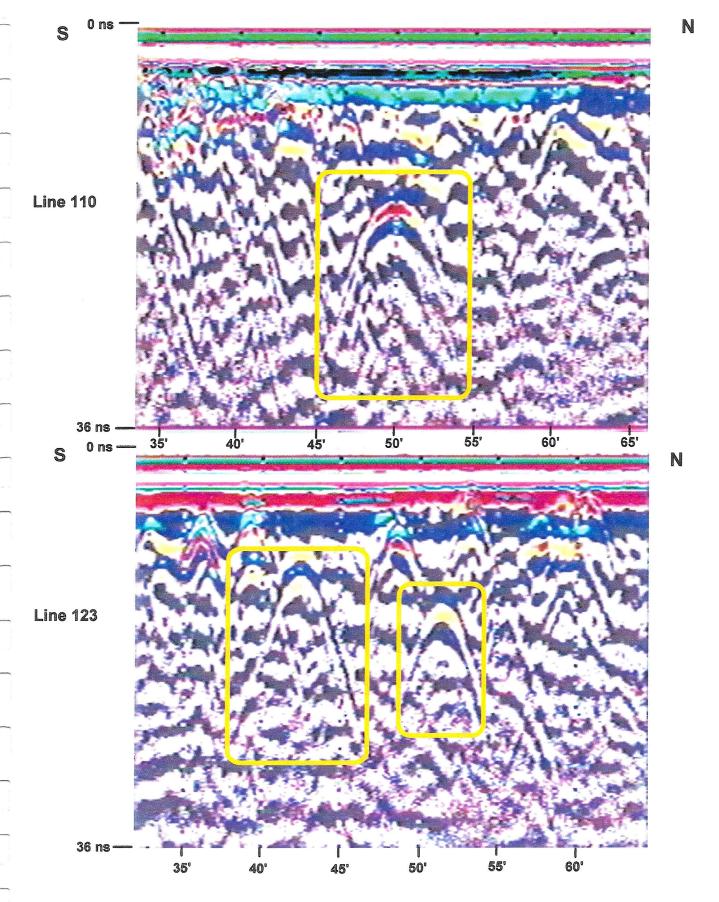


Figure 17. GPR record segments for Line 110 (upper) and Line 123 (lower) east of the walled cemetery, showing major echoes suggesting graves, possibly invaded by tree roots.

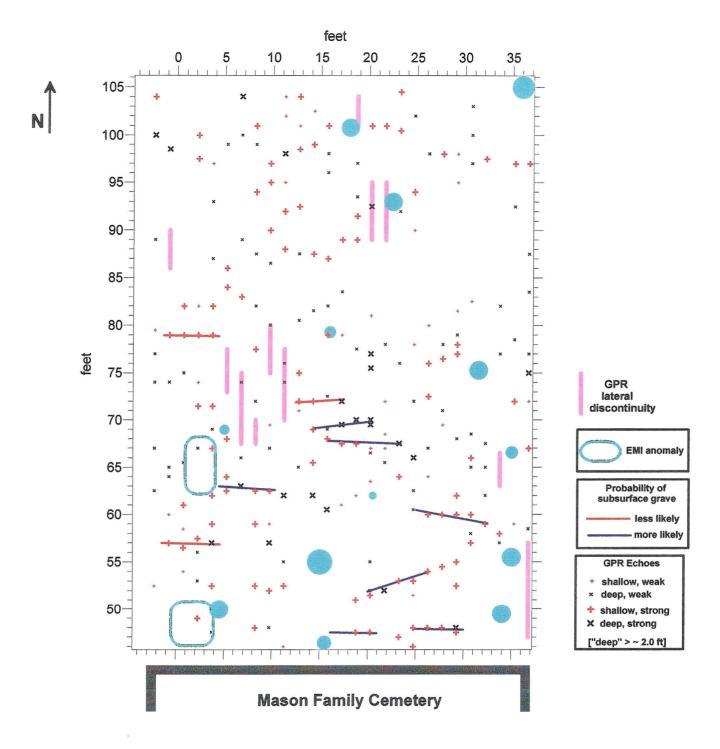


Figure 18. GPR echoes (classified by signal strength and depth), GPR lateral discontinuities, and regions of major EMI anomalies north of the brick-walled cemetery. Echo alignments, which were determined in part by subjective inferences of root-like and grave-like radar signatures, refer to the probability of a grave occurrence.

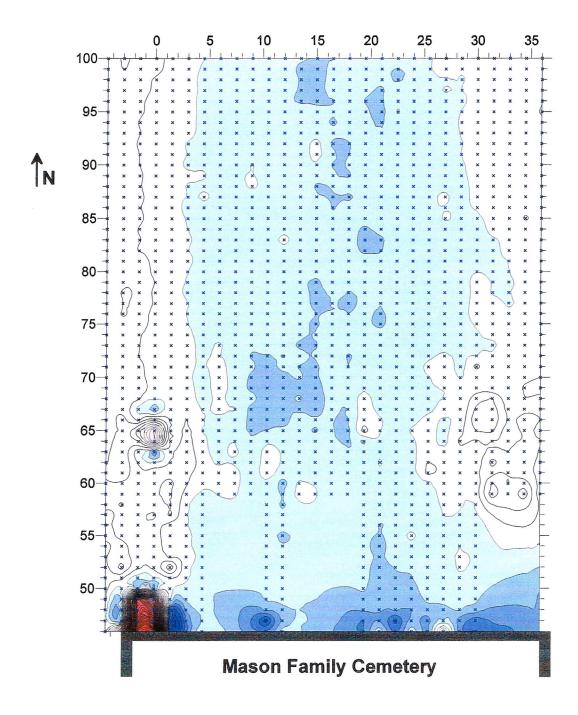


Figure 19. In-phase EMI anomalies over part of the GPR-surveyed area north of the cemetery.

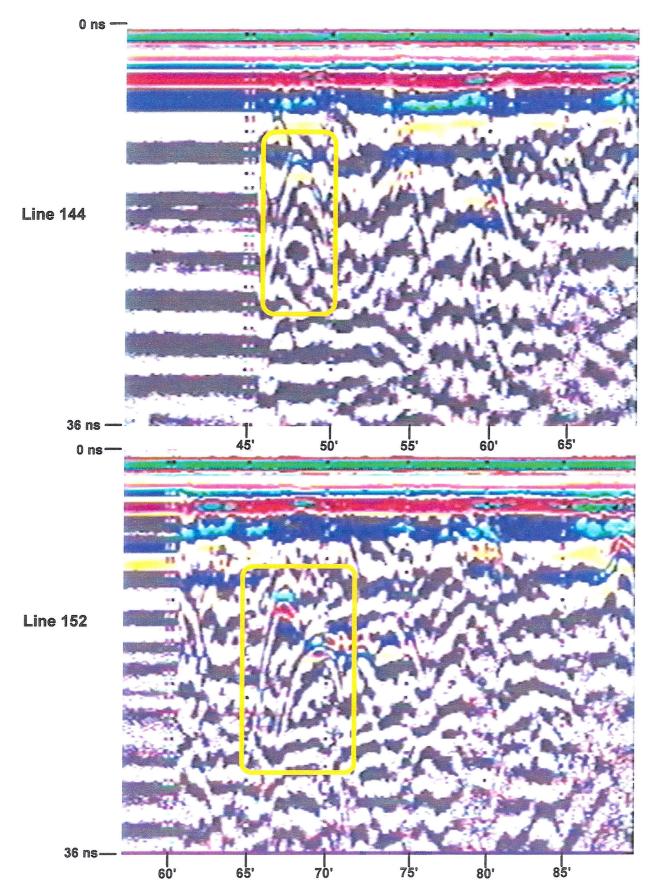


Figure 20. GPR record segments for Line 144 (upper) and Line 152 (lower) north of the walled cemetery, showing major echoes suggesting graves, possibly invaded by tree roots. The echo outlined in yellow on the upper segment (Line 144) shows a circular dark spot, possibly reflecting a void.

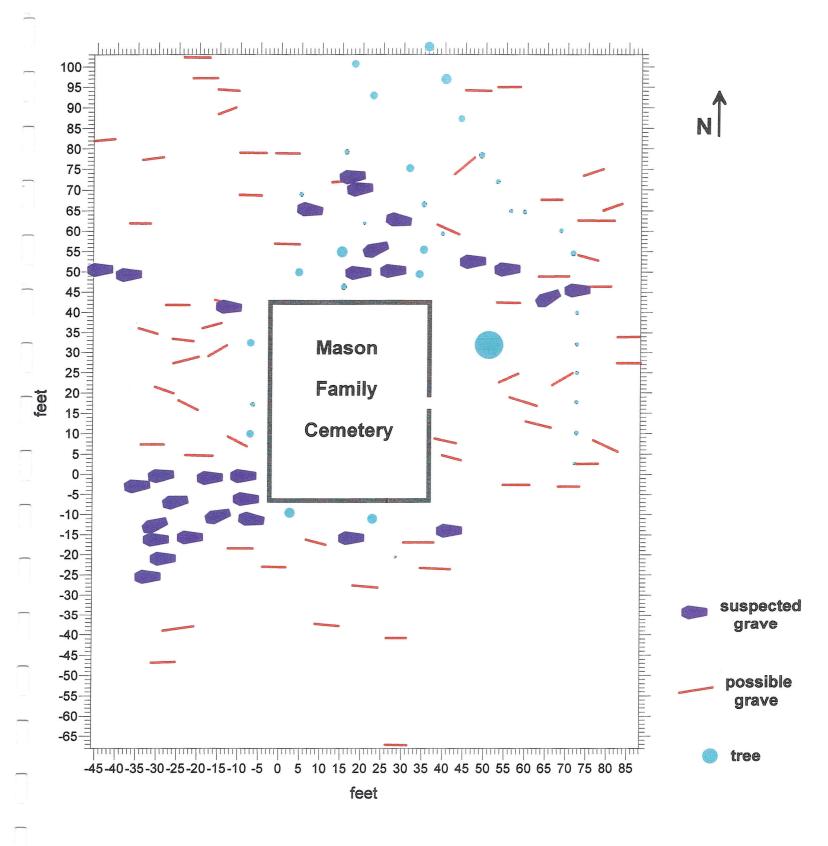


Figure 21. Locations of twenty-nine "suspected graves" and many other "possible graves", commonly also associated with inferred tree roots, outside of the cemetery wall.

#### APPENDIX A

## Data entries for GPR echoes

"Easting" [column 1], and "northing" [column 2] refer, respectively, to distances in feet, increasing eastward and northward relative to the origin of the local coordinate system. Negative values of easting indicate locations west of the coordinate origin. Negative values of northing indicate locations south of the coordinate origin. "2W\_TT" [column 3] refers to the two-way travel time, in nanoseconds, that reflected energy travels from the antenna (as transmitter) to the reflector and back to the antenna (as receiver). This two-way travel time can be converted to depth in feet by assuming a specific value for the velocity of the traveling waves. A velocity of 1/3 ft per nanosecond is a reasonable estimate, in the absence of physical measurements. The heading "signal strength" [column 4] refers to the subjectively estimated amplitude or strength of the returned signal, based on values of 1 (weakest) to 3 (strongest). Comments [column 5] are discretionary. Line numbers [column 6] in increasing sequence correspond to the chronological order in which GPR data were acquired. There is no "Line 151"; this label was inadvertently skipped despite the fact that all lines were run in sequence.

The comments, where added, contain informal abbreviations for characteristics of the signal. Examples are "brd" for broad; "nrrw" for narrow; "brkn" for broken; "Lhf" for left-hand flank of hyperbola; "Rhf" for right-hand flank of hyperbola; "asymm" for asymmetrical; "reverb" for reverberation or ringing of signal; "spot" for localized bright region; and "distort" for distorted.

## Example

For example, the first entry of Appendix A shows that, along GPR Line Number 1, where the center line of the antenna is 36.75 ft east of the coordinate origin, an echo was noted at a distance of 17.0 ft south of the origin. The top of the echo was recorded at a two-way travel-time of 11.0 ns, or one-way travel time of 5.5 ns. If we assume a soil velocity of 1/3 foot per nanosecond, we multiply this velocity by 5.5 ns to obtain an estimated depth to reflector of approximately 1.8 ft. The relative amplitude of this echo was subjectively assigned a value of "3", meaning that it is very strong. There is no comment for this particular entry.

#### APPENDIX B

At the suggestion of Dave Shonyo, we ran GPR and EMI surveys along a 300-ft line extending from coordinate point (-33', 100') in a direction N27°W northwest of the cemetery. The purpose of this reconnaissance line was to test remote-sensing soil conditions in an accessible open area. Historical records imply that slave quarters and "Logtown" existed in this general region but whether it resided in what is now cleared areas or heavily wooded areas remains unknown. The GPR data indicated that radar penetration downward is at least as good as at the cemetery area. Both the GPR and EMI data indicate the subsurface presence of iron pipe conduits (see the 2 associated figures).

Easting (ft) 36.75	Northing (ft) -17.0	2W_TT (ns) 11.0	Signal Strength	Comment	Line Number	Easting (ft) 17.25	Northing (ft) -17.0	2W_TT (ns) 7.0	Signal Strength	Comment	Line Number 14
36.75	-19.0	14.0	1	vague	i	17.25	-25.5	13.0	1	brd	14
36.75	-23.5	6.5	3	nnw	1	17.25	-53.0	13.0	1	brkn_rvrb	14
36.75	-27.5	15.0	1	X-intersect	1	17.25	-62.0	12.0	1		14
36.75	-38.0	12.5	3	brd_RHf	1	15.75	-17.5	32.0	1	brd_chevron	15
36.75	-54.0	11.0	3		1	15.75	-19.0	11.5	1	rvrb	15
35.25	-17.0	9.0	3		2	15.75	-27.5	11.5	1	rvrb	15
35.25	-22.0	6.0	3		2	15.75	-31.0	23.5	1		15
35.25	-23.0	6.0	3		2	15.75	-32.5	21.0	1		15
35.25	-28.0	13.0	1	vague	2	15.75	-34.0	21.0	1		15
35.25	-46.5	11.0	1	nnw	2	15.75	-36.5	17.0	1	chevron	15
33.75	-17.0	11.0	1		3	15.75	-47.5	11.0	1	spot	15
33.75	-18.0	10.0	1		3	15.75	-52.5	17.0	1	brd_brkn	15
33.75	-22.5	13.0	1	nmw	3	15.75	-57.5	12.0	1	brd_rvrb	15
33.75	-32.5	15.5	1	brd_rvrb	3	15.75	-60.5	12.0	1	rvrb .	15
33.75	-38.0	12.5	2 1	brd_rvrb	3 3	14.25	-16.5	8.5 18.0	1	nrrw_rvrb	16
33.75 33.75	-39.0 -54.0	30.0 9.0	1	rvrb brd	3	14.25 14.25	-20.0 -23.0	32.5	1	brd	16 16
32.25	-17.0	7.5	1	biu	4	14.25	-28.0	15.5	1	rvrb_spots	16
32.25	-20.5	8.5	3		4	14.25	-32.5	9.5	1	asymm	16
32.25	-33.0	19.5	2	symm	4	14.25	-38.0	29.0	i	brd_rvrb	16
32.25	-38.0	16.0	1	brd	4	14.25	-43.0	17.0	1	brd	16
32.25	-42.0	16.0	1	distort	4	14.25	-47.0	16.0	i	brd	16
32.25	-62.0	15.5	1		4	12.75	-19.5	31.0	1	chevron	17
30.75	-17.0	7.5	1	RHf	5	12.75	-26.0	28.0	1	brd	17
30.75	-20.5	7.5	3		5	12.75	-37.5	27.0	1	spot	.17
30.75	-29.0	13.0	1	rvrb	5	12.75	-42.5	26.0	1	brd	17
30.75	-33.0	26.5	1	brd_vague	5	12.75	-52.5	25.5	1	brd_brkn	17
30.75	-40.5	19.5	1	vague	5	12.75	-67.5	12.5	1	8	17
30.75	-67.0	13.0	1	brd	5	11.25	-18.0	24.0	1	brd	18
29.25	-29.0	15.0	1	rvrb	6	11.25	-23.0	29.0	1	rvrb	18
29.25	-40.0	19.0	1	brd_rvrb	6	11.25	-31.0	26.0	1	vague	18
29.25	-41.5	20.0	1		6	11.25	-36.5	30.5	1	rvrb	18
29.25	-58.0	22.0	2		6	11.25	-48.5	25.5	1	rvrb	18
29.25	-67.5	5.0	3		6	11.25	-55.0	7.5	1	brd	18
29.25	-72.5	6.0	2	had	6	11.25	-59.0	12.5	1		18
27.75	-30.0 -35.0	17.0 16.5	1	brd_LHfs brkn	7 7	11.25 9.75	-62.5 -17.0	17.5 7.5	1 3	rvrb	18 19
27.75	-35.0 -41.0	7.5	2	rvrb	7	9.75	-25.0	28.0	1	brd_rvrb	19
27.75 27.75	-52.0	20.0	1	nmw	7	9.75	-37.5	21.0	1	DIG_IVID	19
27.75	-58.0	12.0	1	rvrb	7	9.75	-45.0	29.0	1		19
27.75	-67.5	4.5	3	1112	7	9.75	-48.0	22.5	1		19
26.25	-16.0	14.0	1	nrrw_rvrb	8	9.75	-61.0	32.5	1		19
26.25	-17.5	8.0	1	rvrb	8	8.25	-16.5	9.0	2		20
26.25	-18.0	22.0	1		8	8.25	-37.0	32.0	1		20
26.25	-39.0	13.5	1	rvrb	8	8.25	-50.5	22.5	1		20
26.25	-41.0	13.0	1	rvrb	8	8.25	-52.0	26.0	1	brd_rvrb	20
26.25	-51.0	27.0	1	brd_asymm	8	8.25	-68.5	6.5	3	brd	20
26.25	-54.0	15.5	1		8	6.75	-16.0	8.0	2	rvrb	21
26.25	-56.0	10.5	1	rvrb	8	6.75	-25.0	31.5	1	brd	21
26.25	-57.5	13.0	2	brd	8	6.75	-39.0	18.0	1		21
26.25	-63.0	12.0	3 1	had.	8	6.75	-48.0 58.0	9.0 12.5	1	brd_rvrb	21
26.25	-67.0	10.5 15.5	1	brd	9	6.75 6.75	-58.0 -61.5	5.5	3	n.eh	21 21
24.75 24.75	-17.0 -18.0	13.5	1	brd	9	5.25	-24.0	29.5	1	rvrb brd	22
24.75	-23.5	6.5	3	brd	9	5.25	-28.0	28.5	1	rvrb	22
24.75	-62.0	10.0	1	distort	9	5.25	-43.0	31.0	1	rvrb	22
23.25	-17.0	20.5	i	4.0.0.1	10	5.25	-49.0	22.0	1	nrrw_vague	22
23.25	-20.0	12.0	1	brd	10	5.25	-58.5	30.0	1	brd	22
23.25	-25.0	22.5	1	brd	10	3.75	-17.0	22.5	1	vague	23
23.25	-28.0	28.0	1	rvrb	10	3.75	-27.5	30.0	1	rvrb	23
23.25	-33.0	22.0	1	spot	10	3.75	-42.5	24.0	1	brd	23
23.25	-67.0	16.0	1	chevron	10	3.75	-58.0	31.5	1	brd_vague	23
23.25	-67.5	20.5	1	chevron	10	3.75	-62.0	30.5	1	brd	23
21.75	-21.0	10.5	1	RHf	11	2.25	-20.0	6.5	2	brd	24
21.75	-27.5	30.0	1	brd_spot	11	2.25	-21.0	21.5	1	brd_rvrb	24
21.75	-33.5	16.5	1	2	11	2.25	-26.0	23.0	1	rvrb	24
21.75	-47.5	18.5	1	brd_vague	11	2.25	-40.0	24.5	1	brd_spot	24
21.75	-66.5	15.0	2	symm	11	2.25	-44.0	6.5	1	77.3	24
20.25	-17.0	12.0	2		12	2.25	-50.0	11.5	1	brd	24
20.25	-25.5	14.5	1		12	2.25	-57.0	8.5	1	brkn_spot	24
20.25	-28.0	13.5	1		12	2.25	-64.5 17.0	12.0	1	n.eh	24
20.25	-38.0	14.0	1	пп	12	0.75	-17.0	8.5	1	rvrb_symm	25
20.25	-46.5 48.0	17.0	2	bed	12	0.75	-21.0	5.0 12.5	3	rvrb	25
20.25	<b>-48.0</b>	11.5	1	brd	12	0.75	-23.0	12.5	1	spot	25
20.25 20.25	-54.5 -66.5	26.5 20.0	1	brd rvrb	12 12	0.75 0.75	-24.0 -27.0	6.5 27.5	2	brd_rvrb	25 25
18.75	-00.5 -17.0	13.0	1	IVID	13	0.75	-38.5	31.0	1	brd_rvrb	25
18.75	-20.0	10.5	1		13	0.75	-43.0	25.5	i	brd_rvrb	25
18.75	-25.0	14.0	1	brd	13	0.75	-48.5	25.5	i	brd_rvrb	25
18.75	-27.5	25.5	1	brd_vague	13	0.75	-54.5	19.0	1	brd_LHf	25
18.75	-32.5	22.5	1		13	0.75	-68.0	12.0	1	brd_brkn	25
18.75	-54.5	14.0	1	distort	13	-0.75	-17.0	11.0	1	_	26
18.75	<b>-6</b> 8.0	7.0	3		13	-0.75	-22.5	16.0	1	brd_vague	26

Easting (ft) -0.75	Northing (ft) -41.5	2W_TT (ns) 26.0	Signal Strength	Comment	Line Number 26	Easting (ft) -15.75	Northing (ft) -12.5	2W_TT (ns)	Signal Strength	Comment	Line Number
-0.75	-55.0	28.5	1	RHf	26	-15.75	-18.5	11.5	3 1		36 36
-2.25	-15.0	8.0	1	Kili	27	-15.75	-27.0	11.0	1	rvrb	36
-2.25	-18.0	12.0	1		27	-15.75	-38.0	13.0	i	spot	36
-2.25	-21.0	16.5	1		27	-15.75	-42.5	23.0	1	brd	36
-2.25	-23.5	5.0	3	nrrw_rvrb	27	-15.75	-63.0	25.0	1	spot	36
-2.25	-32.5	31.5	1	brd	27	-17.25	0.0	5.5	1	RHfs	37
-2.25	-35.0	14.0	1	rvrb	27	-17.25	-2.5	12.0	1	brkn_spot	37
-2.25	-42.0	20.5	1	brd_rvrb	27	-17.25	-13.0	7.0	3	flanks	37
-2.25	-47.0	14.0	1	brd	27	-17.25	-19.0	6.5	1	na mo	37
-3.75	-3.0	11.5	1	brd	28	-17.25	-24.0	8.5	1		37
-3.75	-8.0	7.0	3	rvrb	28	-17.25	-24.5	5.5	2		37
-3.75	-12.5	6.0	2	rvrb_spot	28	-17.25	-42.0	14.0	1	brd_rvrb	37
-3.75	-15.5	8.0	1	vague	28	-17.25	-45.0	31.0	1	brd	37
-3.75	-23.0	20.5	1	LHf	28	-17.25	-57.0	19.0	1	RHf	37
-3.75	-29.0	5.0	2	spot	28	-17.25	-61.5	21.0	1	brd	37
-3.75	-34.5	30.5	1		28	-18.75	-2.0	5.0	3	rvrb_metall	38
-3.75	-40.0	26.5	1	brd_rvrb	28	-18.75	-7.0	7.0	1	_	38
-3.75	-47.0	28.0	1	brd	28	-18.75	-13.0	7.0	1		38
-3.75	-48.0	31.5	1	brd	28	-18.75	-17.0	11.5	1	rvrb	38
-5.25	-2.0	13.0	1	rvrb_symm	29	-18.75	-18.0	6.0	2	rvrb	38
-5.25	-8.0	8.0	3		29	-18.75	-63.0	17.0	1	brd_spot	38
-5.25	-12.5	6.5	2		29	-20.25	-2.5	17.0	1	spot	39
-5.25	-14.0	6.0	2		29	-20.25	-16.0	10.0	2	flanks	39
-5.25	-16.5	13.0	1		29	-20.25	-17.5	6.5	2		39
-5.25	-29.0	27.5	1	nrrw_rvrb	29	-20.25	-24.0	5.0	1		39
-5.25	-32.5	23.5	1	brd	29	-20.25	-32.0	11.0	. 1		39
-5.25	-53.5	16.5	1		29	-20.25	-37.5	10.0	1		39
-6.75	-2.0	15.0	1	nrrw_rvrb	30	-20.25	-45.0	18.0	1		39
-6.75	-3.0	11.5	1	rvrb_RHfs	30	-21.75	-7.5	6.5	2	rvrb	40
-6.75	-5.5	5.0	2	brd_RHf	30	-21.75	-13.0	6.0	2	nrrw_rvrb	40
-6.75	-7.5	14.0	1	brd	30	-21.75	-17.0	7.5	1	rvrb	40
-6.75	-12.0	6.5	3	rvrb	30	-21.75	-24.0	12.5	1		40
-6.75	-17.0	12.5	1	symm	30	-21.75	-27.5	6.5	1	spot_vague	40
-6.75	-18.5	5.0	1		30	-21.75	-38.0	5.0	1	nrrw_brkn	40
-6.75	-23.0	5.0	1		30	-21.75	-62.0	26.0	1	brd	40
-6.75	-30.5	24.0	1	brd_rvrb	30	-23.25	-1.0	9.5	2	nmw_spot	41
-6.75	-40.0	26.0	1	brd_rvrb	30	-23.25	-7.0	6.5	1		41
-6.75	-52.0	15.0	1	brd	30	-23.25	<b>-</b> 8.0	11.5	1	brd_LHf	41
-8.25	-1.0	6.5	2	RHfs	31	-23.25	-16.5	6.0	3	rvrb	41
-8.25	-6.0	5.5	2		31	-23.25	-39.0	5.0	2	nrw_rvrb	41
-8.25	-8.5	7.5	1	rvrb_distort	31	-24.75	-1.5	13.0	1	RHfs	42
-8.25	-11.0	6.5	2		31	-24.75	-6.5	15.0	1	spot	42
-8.25	-15.0	4.0	1		31	-24.75	-8.0	16.0	1	spot	42
-8.25	-18.5	5.0	1		31	-24.75	-8.5	6.5	1		42
-8.25	-22.5	5.0	1		31	-24.75	-13.0	12.5	1	brd_brkn	42
-8.25	-37.5	26.5	1	brd	31	-24.75	-17.0	6.0	1		42
-8.25	-40.0	29.0	1	brd	31	-24.75	-19.0	6.5	1	nrw_brkn	42
-8.25	-52.5	30.0	1	brd_brkn	31	-24.75	-22.0	6.5	1	RHfs	42
-9.75	-2.0	14.0	1	spot	32	-24.75	-24.0	12.5	1	spot	42
-9.75 -9.75	-4.5 -7.0	7.0 5.5	1 3	brkn	32 32	-24.75 -24.75	-38.0 -52.5	6.5 25.5	1	had a de	42 42
-9.75	-11.0	5.0	3		32	-26.25	-2.5	10.0	2	brd_rvrb brd	43
-9.75	-12.0	6.5	2		32	-26.25	-8.5	9.0	1	spot	43
-9.75	-18.0	9.5	2		32	-26.25	-13.0	7.0	2	rvrb	43
-9.75	-25.5	10.0	1		32	-26.25	-17.0	6.5	2		43
-9.75	-32.0	32.0	1		32	-26.25	-22.0	6.0	2		43
-9.75	-40.0	31.0	1		32	-26.25	-27.0	7.5	2	rvrb	43
-9.75	-53.0	21.5	1	brd_rvrb	32	-26.25	-39.0	6.0	2	brd	43
-11.25	-2.0	20.0	1	spot	33	-26.25	-45.0	13.0	1	brd	43
-11.25	-7.0	13.0	1	nrw_rvrb	33	-27.75	-2.5	7.5	1	rvrb	44
-11.25	-8.0	13.0	1	brd	33	-27.75	-3.5	11.0	2	brd	44
-11.25	-10.5	5.5	3	metall	33	-27.75	-5.5	9.5	2	g?	44
-11.25	-12.0	6.0	2		33	-27.75	-8.5	9.0	1	spot	44
-11.25	-18.0	11.5	2		33	-27.75	-13.5	5.5	3	brd_spot	44
-11.25	-28.5	26.5	1	brd_vague	33	-27.75	-17.0	7.0	3	brd_RHfs	44
-11.25	-57.0	6.5	2	-	33	-27.75	-18.5	8.0	1	_	44
-11.25	-62.0	22.0	1	brd_rvrb	33	-27.75	-21.0	4.5	2		44
-12.75	-2.5	14.0	1	brd_rvrb	34	-27.75	-25.5	4.0	2	rvrb	44
-12.75	-8.0	30.5	1	_	34	-27.75	-27.5	11.0	1	brkn	44
-12.75	-11.5	5.5	3		34	-27.75	-35.5	8.0	1	rvrb	44
-12.75	-18.0	7.0	1		34	-27.75	-39.0	6.0	2		44
-12.75	-19.0	12.5	1		34	-27.75	-46.0	8.5	1		44
-12.75	-23.0	32.5	1	chevron	34	-27.75	-48.0	6.0	2		44
-12.75	-37.0	29.0	1	brd	34	-27.75	-55.0	17.5	1	brd_rvrb	44
-12.75	-47.0	32.0	1	chevron	34	-29.25	-3.0	6.5	3	rvrb_asymm	45
-12.75	-57.0	35.0	1	brd_rvrb	34	-29.25	-5.0	6.5	2	brkn	45
-14.25	-2.5	21.0	1	brd	35	-29.25	-7.0	7.0	1	rvrb	45
-14.25	-6.5	4.0	1	chevron	35	-29.25	-14.0	5.5	3		45
-14.25	-11.5	4.5	2		35	-29.25	-16.5	17.5	. 1	rvrb	45
-14.25	-14.0	15.0	1	chevrons	35	-29,25	-17.0	8.5	2	rvrb	45
-14.25	-17.0	24.0	1	brd	35	-29.25	-18.0	8.5	2		45
-14.25	<b>-4</b> 5.5	29.0	1	brd_RHf	35	-29.25	-22.5	31.5	1	brd	45
-15.75	-2.5	16.5	1	spot	36	-29.25	-28.0	7.0	1	vague	45

Easting (ft)	Northing (ft)	2W_TT (ns)	Signal Strength	Comment	Line Number	Easting (ft) 51.75	Northing (ft) -26.0	2W_TT (ns) 4.0	Signal Strength	Comment	Line Number 60
-29.25	-30.0	21.0	1	brd_rvrb	45 45	53.25	-5.0	26.0	1	nrww_rvrb brd_rvrb	61
-29.25	-37.0	28.0	1	rvrb	45	53.25	-13.0	5.0	3	brkn	61
-29.25	-40.0	25.0		brd_vague	45	53.25	-17.0	16.0	2	DIKII	61
-29.25	<b>-46.0</b>	27.0	1	brd brd arth	45	54.75	-2.5	14.0	1	brd	62
-29.25	-53.0	18.0	1	brd_rvrb	45 46	54.75	-2.5 -12.5	19.0	1	brd_rvrb	62
-30.75	-2.5	14.0	1	nnw_rvrb	46	54.75	-20.0	25.5	1	brd_rvrb	62
-30.75	<b>-4.0</b>	10.0	2	nmw_rvrb	46	56.25	-3.0	6.0	1	brd_brkn	63
-30.75	-7.0	7.5	1					23.0	1		64
-30.75	-12.0	8.0	1	spot	46	56.25	-5.5			rvrb	
-30.75	-14.0	7.0	2		46	56.25	-13.0	13.5	1		64
-30.75	-17.0	10.0	2		46	57.75	-2.5	10.5	1	had and	64
-30.75	-22.0	5.0	2		46	57.75	-15.0	24.0	1	brd_rvrb	64
-30.75	-23.5	22.0	1	rvrb	46	59.25	-2.5	23.0	1	1000	65
-30.75	-27.0	9.0	1	brd_asymm	46	59.25	-13.0	14.0	1	rvrb	65
-30.75	-34.0	7.0	1	chevrons	46	59.25	-14.0	11.0	1		65
-30.75	-37.5	28.0	1	brd_rvrb	46	60.75	-3.0	23.0	1	brd_rvrb	66
-30.75	-47.5	26.0	1	brd_rvrb	46	60.75	-9.0	6.0	1 .	nnw_asymm	66
-32.25	-3.0	8.5	3	rvrb	47	60.75	-15.0	9.0	1	RHfs	66
-32.25	-6.0	10.5	1		47	62.25	-5.0	25.0	1	brd_vague	67
-32.25	-15.0	9.0	2	brd_flanks	47	63.75	-5.5	21.0	1	brd_vague	68
-32.25	-17.0	8.0	2	flanks	47	65.25	-3.0	21.0	. 1	brd_rvrb	69
-32.25	-25.0	9.5	1		47	65.25	-12.5	8.0	1		69
-32.25	-27.5	10.0	1	brkn	47	66.75	-4.0	4.0	3		70
-32.25	-31.0	6.5	- 1	rt?	47	66.75	-13.0	6.0	3	brd_rvrb	70
-32.25	-37.5	7.0	1	RHf	47	68.25	-3.0	5.0	1	chevrons	71
-33.75	-4.0	7.5	3	brkn	48	68.25	<b>-4</b> .0	3.5	2		71
-33.75	-7.5	21.0	1	brd_rvrb	49	68.25	-7.0	23.0	1	brd_rvrb	71
-33.75	-15.5	6.5	2	rvrb_LHfs	49	69.75	-2.5	18.0	1	RHfs	72
-33.75	-17.0	6.5	2	rvrb	49	69.75	-5.0	10.0	1		72
-33.75	-19.0	7.5	1	RHf	49	71.25	-3.0	12.0	1	brd_brkn	73
-33.75	-26.0	6.0	2		49	72.75	-3.0	5.0	3		74
-35.25	-5.0	11.5	2	brd_rvrb	49	-3.75	1.0	5.0	3	nrrw_rvrb	75
-35.25	-26.5	6.5	2	brd	49	-3.75	2.5	7.5	1	utiw_tvtp	75
-36.75	-5.5	8.0	2	brd_rvrb	50	-3.75	4.0	7.5	1	rvrb	75
-36.75	-10.0	18.0	1	brd_rvrb	50	-3.75	7.5	11.5	1		75
-36.75	-22.0	4.5	2	rt?	50	-3.75	14.0	15.5	1	brd_vague	75
-36.75	-26.0	5.0	2	g?/rt?	50	-3.75	26.0	6.5	1	brd_chevron	75
38.25	-15.0	5.5	2	RHfs	51	-3.75	32.5	11.0	2		75
38.25	-24.0	6.0	2		51	-3.75	36.5	10.0	2		75
38.25	-25.0	18.0	1	brd_rvrb	51	-3.75	43.0	4.5	3	rvrb	75
38.25	-40.0	17.5	2	brd	51	-3.75	49.0	11.5	1	RHf_vague	75
38.25	-43.0	14.0	2	RHfs	51	-3.75	53.0	15.5	1	brd	75
38.25	-54.0	11.0	2	asymm	51	-3.75	64.0	4.5	3	nrrw_rvrb	75
39.75	-15.5	6.5	3	3	52	-3.75	73.5	11.5	2	brd	75
39.75	-23.0	8.5	1		52	-3.75	79.0	7.5	2		75
39.75	-26.0	4.5	3		52	-3.75	87.5	11.5	2	brd	75
41.25	-8.5	21.0	1 .	brd	53	-5.25	2.0	16.5	1	brd_RHf	76
41.25	-15.0	6.0	2		53	-5.25	3.0	9.0	1	rvrb	76
41.25	-23.0	6.5	2		53	-5.25	6.5	5.5	1	brd_rvrb	76
41.25	-26.5	6.5	2		53	-5.25	9.5	5.5	2		76
42.75	-4.0	7.5	1	LHf	54	-5.25	17.5	8.0	- 1	brd_chevron	76
42.75	-14.5	14.0	1	brd_rvrb	54	-5.25	22.5	12.0	1	brd_vague	76
42.75	-21.0	24.5	1	brd_rvrb	54	-5.25	26.0	13.0	2		76
42.75	-38.0	11.5	1	_	54	-5.25	26.5	12.5	1	brd_RHf	76
42.75	-44.0	14.0	1	brkn	54	-5.25	28.0	11.0	1		76
44.25	-2.5	6.5	1	vague	55	-5.25	29.0	8.0	1	nrrw_rvrb	76
44.25	-8.5	25.0	1	brd_rvrb	55	-5.25	32.5	11.0	1	rvrb	76
44.25	-16.0	12.0	1	rvrb	55	-5.25	35.0	7.0	2	nrrw_rvrb	76
44.25	-20.0	29.5	1	rvrb	55	-5.25	41.5	8.0	2	brd_rvrb	76
44.25	-28.0	24.0	1		55	-5.25	54.0	24.0	1	brd_rvrb	76
44.25	-47.5	11.0	1	spot	55	-5.25	61.5	25.0	- 1	nrw_rvrb	76
44.25	-52.0	10.0	2		55	-5.25	64.0	6.5	2	rvrb	76
45.75	-5.0	5.0	2		56	-5.25	69.0	23.5	1	nrrw_rvrb	76
45.75	-7.0	5.5	2	RHf	56	-5.25	69.5	32.5	1	<del>-</del>	76
45.75	-14.0	5.5	3		56	-5.25	72.0	30.0	1		76
45.75	-26.0	18.0	1	rvrb_distort	56	-5.25	80.0	7.0	2	r?	76
45.75	-37.0	16.5	1	brd	56	-5.25	85.0	12.0	2	brd_rvrb	76
47.25	-2.5	14.0	i	brd_rvrb	57	-5.25	92.0	28.0	1	brd_rvrb	76
47.25	-8.0	11.5	2	2.0	57	-5.25	96.0	18.5	1	brd_rvrb	76
47.25	-12.5	13.5	1	rvrb	57	-6.75	1.0	8.0	1	chevrpns	77
47.25	-20.0	28.0	1	1415	57	-6.75	3.0	10.0	1	chevron_RHf	77
47.25	-26.0	10.0	2	brd	57	-6.75	26.5	14.0	i	RHf	77
47.25	-33.0	18.5	1	rvrb	57	-6.75	37.5	32.0	1	brd_vague	77
47.25	-33.0 -41.5	18.0	1	nrw_rvrb	57	-6.75	39.0	17.0	i		77
	-8.0	18.5	1	IIIIM_IAID	58	-6.75	42.0	7.0	2	brd_rvrb	77
48.75		17.5	1	brd	58	-6.75	45.0	5.5	2	brd_rvrb	77
48.75	-22.5	16.0	1		58	-6.75	47.0	10.5	1	J. 4.10	77
48.75	-42.0		1	asymm rvrb_vagie	59	-6.75	50.0	26.0	i	brd_rvrb	77
50.25	-2.5	17.5			59	-6.75 -6.75	57.0	13.0	2	brd_brkn	77
50.25	-9.5 13.0	18.0	1	prd_rvrp	59 59	-6.75	63.5	10.0	1	nrw	77
50.25	-13.0	7.0	2	hed such	59 59	-6.75	69.5	10.0	1	rvrb	77
50.25	-21.0	21.5	1	brd_rvrb	59 59	-6.75 -6.75	73.0	18.0	1	brd	77
50.25	-31.0	8.0	1	rvrb	60	-6.75	79.5	5.5	3	Did	77
51.75	-2.5	12.0	1	brd_rvrb		-6.75	92.0	25.5	1	brd_chevron	77
51.75	-21.0	30.0	1		60	-0.75	92.U	20.0		24 TO 1011	

Easting (ft)	Northing (ft)	2W_TT (ns)	Signal Strength	Comment	Line Number	Easting (ft)	Northing (ft)	2W_TT (ns)	Signal Strength	Comment	Line Number
-8.25	2.5	11.0	1	RHf	78	-15.75	43.0	15.0	1	brd_spot	83
-8.25	7.0	11.5	2	brd	78	-15.75	46.0	7.5	2	brd	83
-8.25 -8.25	11.0 13.5	8.0 12.0	2 1	brd brd_RHf	78 78	-15.75 -15.75	47.0 58.0	30.5 6.0	1	rvrb	83
-8.25	25.0	12.5	i	brd_rvrb	78	-15.75	64.0	22.0	1	chevron	83 83
-8.25	31.0	6.0	3	nrrw_rvrb	78	-15.75	72.5	28.5	1	rvrb brd_rvrb	83
-8.25	33.0	5.5	3	nrrw_rvrb	78	-15.75	82.0	13.5	1	DIG_IVID	83
-8.25	38.0	19.5	1	LALP	78	-15.75	87.5	12.5	2	rvrb	83
-8.25	39.0	13.0	2	brd	78	-15.75	89.0	14.0	1	LHf_vague	83
-8.25	40.0	7.0	1	Did	78	-15.75	95.0	2.5	3	nrw_rvrb	83
-8.25	48.5	5.5	2	nrrw_rvrb	78	-15.75	97.0	11.0	1	spot	83
-8.25	52.5	5.0	3	nrrw_rvrb	78	-15.75	98.0	11.0	1	Spot	83
-8.25	67.5	18.0	1	brd_rvrb	78	-15.75	100.0	21.0	1	brd_LHf	83
-8.25	76.0	24.0	1	brd_rvrb	78	-17.25	1.0	6.5	i	nrw	84
-8.25	78.5	8.0	1	-	78	-17.25	4.5	9.0	3	brd_flanks	84
-8.25	82.5	30.0	1	brd_rvrb	78	-17.25	6.0	10.0	2	brd_RHf	84
-8.25	93.0	24.0	1	brd chevrons	78	-17.25	29.0	9.5	3	brd_rvrb	84
-9.75	2.5	6.0	1	rvrb	79	-17.25	33.5	12.5	1	brd_vague	84
-9.75	3.5	16.5	1		79	-17.25	36.5	10.0	2	rvrb	84
-9.75	8.0	10.0	2	brd	79	-17.25	37.5	13.5	1	rvrb	84
-9.75	11.0	6.5	1	brd_RHf	79	-17.25	38.0	31.0	1	brd	84
-9.75	16.0	12.5	1	brd_rvrb	79	-17.25	58.0	17.0	1	brkn_spot	84
-9.75	20.0	13.0	1	brd	79	-17.25	70.0	31.5	1	brd_spot	84
-9.75	27.0	11.5	1	brd_rvrb	79	-17.25	72.5	31.0	1	spot	84
-9.75	38.5	3.5	3		79	-17.25	85.0	31.0	1	brd_chevron	84
-9.75	44.5	9.5	1	brd_RHf	79	-17.25	91.0	31.0	1	spot_vague	84
-9.75	68.5	32.5	1	brd_symm	79	-17.25	96.5	31.5	1		84
-9.75	78.5	8.0	2	brd	79	-17.25	100.0	17.0	1	brd_LHfs	84
-9.75	83.0	8.0	1	brd	79	-18.75	1.5	7.0	2	nrw	85
-9.75	87.0	13.0	2	brd_distort	79	-18.75	5.5	7.0	2	brd_rvrb	85
-9.75	91.0	22.0	1	brd	79	-18.75	20.0	16.5	1		85
-11.25	2.0	9.0	1	nrw	80	-18.75	21.0	15.0	1	to a con-	85
-11.25	8.5	10.0	2 2	brd	80 80	-18.75	28.0 35.0	7.0 14.0	3 1	brd_rvrb	85
-11.25	11.0	6.5 17.0	1	brd_rvrb	80	-18.75 -18.75	36.0	6.5	2	RHf	85 85
-11.25	20.0		3	brd_vague	80			6.0	3	non u nuch	
-11.25	30.5 33.0	5.0 10.0	2	rvrb -	80	-18.75 -18.75	45.0 63.0	24.0	1	nmw_rvrb	85 85
-11.25	35.0	9.5	2	r? brd_RHf	80	-18.75	79.0	11.0	1	rvrb	85
-11.25 -11.25	39.0	5.0	3	rvrb	80	-18.75	83.0	31.0	1	brd	85
-11.25	42.0	14.0	2	brd_RHf	80	-18.75	92.5	32.5	1	chevron	85
-11.25	47.0	19.0	1	brd_chevron	80	-18.75	97.5	30.0	i	brd	85
-11.25	58.0	14.0	i	brd_chevrons	80	-18.75	99.5	20.5	1	brd_LHf	85
-11.25	90.0	23.0	i	brd_rvrb	80	-18.75	102.5	20.0	i	brd_rvrb	85
-11.25	94.0	18.0	1	2.0	80	-20.25	1.5	6.5	2	nrrw	86
-12.75	2.0	9.0	1		81	-20.25	5.0	8.0	3	RHf	86
-12.75	9.5	11.0	3		81	-20.25	7.5	10.0	1	RHf	86
-12.75	20.0	18.5	1	rvrb	81	-20.25	16.0	18.0	1	brd	86
-12.75	28.0	13.0	1		81	-20.25	21.0	11.0	1	brd_rvrb	86
-12.75	32.0	8.0	3	rvrb	81	-20.25	24.0	11.0	1	brkn_vague	86
-12.75	35.5	12.0	3	brd	81	-20.25	29.0	6.5	3	Г	86
-12.75	39.5	6.0	3	rvrb	81	-20.25	37.0	5.0	2	r	86
-12.75	42.0	26.5	1	brd	81	-20.25	38.0	12.0	1	brd_brkn	86
-12.75	50.0	31.5	1	brd_vague	81	-20.25	42.0	21.0	1	brd	86
-12.75	65.0	32.0	1	brd	81	-20.25	78.0	10.0	1	brkn	86
-12.75	77.0	9.0	2	brd_symm	81	-20.25	82.5	31.0	1	brd	86
-12.75	90.0	23.0	1	brd_LHfs	81	-20.25	98.0	22.5	1	brd	86
-12.75	94.0	22.5	1	brd_spot	81	-20.25	101.5	18.0	1	brd	86
-14.25	2.0	8.5	2 1	rvrb	82	-21.75	4.0	7.0	2	nrrw	87
-14.25	3.0	10.5	1		82	-21.75	5.0	10.0	1	nrw_rvrb	87
-14.25	7.0	11.0	2	brd_rvrb	82	-21.75	5.5	6.0	3	nrrw_rvrb	87
-14.25	22.0	5.0	2		82	-21.75	7.0	12.0	1		87
-14.25	27.5	5.0	3	rvrb	82	-21.75	7.5	21.0	1	spot	87
-14.25	32.0	12.5	3	brd	82	-21.75	12.5	8.0 10.0	2	LHfs	87
-14.25	37.0	12.5 6.5	2 1	RHf	82 82	-21.75 -21.75	17.0 19.0	6.5	2	chevron	87
-14.25	39.0 <b>4</b> 3.0	10.0	2	brkn	82	-21.75 -21.75	23.5	11.0	1	r brd	87 87
-14.25 -14.25	46.5	11.5	2	DIKII	82	-21.75	28.5	10.0	2	rt	87
-14.25	64.0	6.0	1	brd	82	-21.75	29.5	7.0	2	r	87
-14.25	80.0	13.0	i	brd_LHf	82	-21.75	30.5	14.5	1	'	87
-14.25	83.0	28.5	1	brd_brkn	82	-21.75	32.5	14.0	2	rvrb	87
-14.25	88.5	29.0	i	brkn	82	-21.75	42.5	24.0	1	1415	87
-14.25	92.5	26.5	1	vague	82	-21.75	52.0	10.0	1	vague	87
-14.25	95.0	27.0	1	, 0,300	82	-21.75	55.0	30.0	1	brd	87
-14.25	97.0	16.0	1	LHfs	82	-21.75	62.5	11.0	i	brd	87
-15.75	2.0	8.0	i	nmw_rvrb	83	-21.75	72.0	13.0	1		87
-15.75	3.0	11.5	i		83	-21.75	77.0	10.5	1	brkn	87
-15.75	7.0	7.5	3	rvrb	83	-21.75	97.5	11.5	1	brd	87
-15.75	8.5	11.5	2		83	-21.75	102.0	18.0	1		87
-15.75	18.0	12.5	1	asymm_spot	83	-21.75	102.5	10.0	1		87
-15.75	22.0	10.5	1	brd_brkn	83	-23.25	2.0	9.5	1	nrrw	88
-15.75	24.0	12.5	1	rvrb_vague	83	-23.25	3.0	4.5	3	nrrw_rvrb	88
-15.75	30.5	9.0	3	brd_RHf	83	-23.25	5.0	10.0	1	=	88
-15.75	37.5	7.5	2	rvrb	83	-23.25	7.0	9.0	1	chevron	88
-15.75	39.5	14.0	1	flanks	83	-23.25	17.0	27.0	1	RHf	88

Easting (ft)	Northing (ft)	2W_TT (ns)	Signal Strength	Comment	Line Number	Easting (ft)	Northing (ft)	2W_TT (ns)	Signal Strength	Comment	Line Number
-23.25	18.0	18.5	1	brd_rvrb	88	-30.75	87.5	10.0	1	rvrb	93
-23.25	28.5	6.0	3	LHf	88	-32.25	2.0	9.0	1	nrrw	94
-23.25	33.5	12.0	1	LHf	88	-32.25	3.5	10.0	2		94
-23.25	38.0	10.0	1		88	-32.25	7.5	7.0	1	10	94
-23.25	42.0	7.5	2	100	88	-32.25	14.0	11.0	1	rvrb	94
-23.25	59.0	18.0	1	chevron_spot	88	-32.25	23.0	17.5	1		94
-23.25	78.5	28.0	1	chevron_spot	88	-32.25	27.0	9.0	2		94
-23.25	89.0	28.0	1	brd_rvrb	88	-32.25	35.5	10.0	1	brd	94
-23.25	96.5	15.5	1	brd_RHf	88	-32.25	45.0	8.0	2	LALP	94
-23.25	102.0	16.0	1	brd	88	-32.25	62.0	11.5	1	rvrb	94
-24.75	2.0	10.0	. 1	nrrw_revrb	89	-32.25	62.5	11.0	1	RHf	94
-24.75	3.0	8.5	2	brd_rvrb	89	-32.25	78.0	7.5	1		94
-24.75	13.5	11.5	1	brd	89	-32.25	102.0	20.0	1	brd	94
-24.75	18.5	10.5	3		89	-33.75	1.5	11.0	1	nrrw	95
-24.75	27.0	18.0	1	brd_spot	89	-33.75	3.5	9.5	2	f?_r?	95
-24.75	27.5	8.0	2		89	-33.75	7.5	7.0	1		95
-24.75	33.5	10.0	1	rvrb_spot	89	-33.75	10.0	16.0	1	brd	95
-24.75	39.0	9.0	2	rvrb	89	-33.75	11.5	7.5	1	rvrb	95
-24.75	41.0	9.0	3	rvrb	89	-33.75	17.0	8.0	1	rvrb	95
-24.75	50.0	10.0	1	chevron_LHf	89	-33.75	22.0	9.0	1	rvrb	95
-24.75	61.0	14.5	1	chevrons	89	-33.75	27.5	9.0	. 1		95
-24.75	73.0	23.0	1 .	brd_rvrb	89	-33.75	28.0	11.0	1	spot	95
-24.75	78.0	25.0	1		89	-33.75	36.0	16.5	1		95
-24.75	80.0	14.0	1	brd	89	-33.75	46.5	11.0	2	brd_rvrb	95
-24.75	97.0	23.5	1	brd	89	-33.75	52.5	11.0	1	rvrb	95
-24.75	100.5	22.0	1	RHf	89	-33.75	62.5	12.5	1	RHfs	95
-26.25	1.0	8.0	1	ппъ	90	-33.75	67.5	10.5	1	RHfs	95
-26.25	2.5	10.5	3	RHf	90	-33.75	77.5	8.0	2		95
-26.25	4.0	8.0	1		90	-33.75	98.0	7.5	1	rvrb	95
-26.25	20.0	9.5	3		90	-35.25	32.0	27.5	1		96
-26.25	24.0	12.0	1		90	-35.25	37.0	21.5	1	brd_RHf	96
-26.25	27.5	11.5	1		90	-35.25	47.5	11.0	1 -	-	96
-26.25	33.5	7.0	2		90	-35.25	52.5	12.0	1		96
-26.25	36.5	10.0	1		90	-35.25	62.5	12.0	1	spot	96
-26.25	42.0	7.5	2		90	-35.25	72.5	12.0	. 1	RHf	96
-26.25	44.0	8.0	1	rvrb	90	-35.25	85.5	22.0	1	LHf	96
-26.25	49.0	31.0	1	brd	90	-36.75	42.5	11.5	2	rvrb	97
-26.25	52.0	5.0	2	nrrw_rvrb	90	-36.75	47.0	11.0	2	rvrb	98
-26.25	58.0	18.0	1	rvrb	90	-36.75	59.0	9.0	1	nrw	98
-26.25	62.0	16.0	1	spot	90	-36.75	61.5	11.0	1		98
-26.25	70.0	8.0	1	ппw	90	-36.75	87.0	30.0	1	brd	98
-26.25	73.0	13.0	. 1	spot_vague	90	-36.75	93.0	12.0	. 1	brd	98
-26.25	87.5	8.0	1	nnw	90	-36.75	101.5	27.0	1	brd	98
-26.25	94.0	24.5	1	brd	90	-38.25	37.0	24.0	1	brd_rvrb	98
-26.25	103.0	21.0	1	brd	90	-38.25	47.0	9.5	1	chevrons	98
-27.75	2.0	10.0	2		91	-38.25	52.0	10.0	1	nrrw_rvrb	98
-27.75	3.5	7.5	1 .	r?	91	-38.25	70.0	11.5	1	RHfs	98
-27.75	6.0	8.0	1		91	-38.25	77.0	11.0	1	RHf	98
-27.75	16.5	12.0	1	brd	91	-38.25	87.0	6.0	1		98
-27.75	20.5	13.0	1	nnw_rvrb		-38.25	93.0	10.0	1		98
-27.75	26.0	9.0	1		91	-38.25	100.5	29.5	1	brd	98
-27.75	42.0	8.5	2	brd_rvrb	91	-39.75	36.5	8.0	1		99
-27.75	53.0	31.5	1	brd	91	-39.75	47.0	7.5	2	flanks	99
-27.75	69.0	7.0	2	nrrw_rvrb	91	-39.75	60.0	10.5	1	chevron	99
-27.75	90.5	10.0	1	brd	91	-39.75	77.0	29.5	1	brd_rvrb	99
-27.75	98.0	13.0	1	chevron	91	-39.75	90.0	29.0	1	brkn_vague	99
-27.75	101.0	23.5	1	brd	91	-41.25	32.5	20.0	1	nrrw_rvrb	100
-27.75	103.0	27.0	1	brd_chevrons	91	-41.25	46.0	22.0	1	rvrb	100
-29.25	2.0	10.0	2	brd	92	-41.25	48.0	9.0	3	brd_rvrb	100
-29.25	7.0	8.0	1	rvrb	92	-41.25	60.0	11.0	1	rvrb	100
-29.25	8.0	8.0	1		92	-41.25	82.5	5.5	1		100
-29.25	21.0	20.5	1	brd	92	-41.25	88.5	9.5	1	brd_brkn	100
-29.25	42.5	10.0	2	brd	92	-41.25	100.0	10.5	1	brkn_chevron	100
-29.25	45.5	8.0	1	spot	92	-42.75	35.0	10.5	1		101
-29.25	57.0	32.0	1	nrw	92	-42.75	46.0	10.5	1		101
-29.25	61.0	13.0	1		92	-42.75	48.5	8.5	1	LHf	101
-29.25	67.5	30.0	1	brd	92	-42.75	65.0	21.5	1	spot	101
-29.25	75.0	16.5	1		92	-42.75	67.0	4.0	2 1		101
-29.25	78.0	13.0	1		92	-42.75	71.0	20.5		rvrb	101
-29.25	87.5	7.5	2	1?	92	-42.75	78.0	7.0	1		101
-29.25	95.0	26.0	1	rvrb	92	-42.75	82.0	6.5	2	gs orang	101
-30.75	2.0	6.5	1	LHf	93	-42.75	88.5	10.5	1	rvrb_LHfs	101
-30.75	3.5	8.0	2		93	-42.75	95.0	28.0	1	brd	101
-30.75	7.5	7.0	1		93	-42.75	97.5	31.0	1	200000000000000000000000000000000000000	101
-30.75	18.0	18.5	1		93	-42.75	102.0	5.0	2	rvrb	101
-30.75	21.5	14.5	1		93	-42.75	104.0	4.5	2	rvrb	101
-30.75	35.0	18.0	1	vague	93	-44.25	34.0	11.0	1	nrw_vague	102
-30.75	40.0	14.0	1		93	-44.25	39.0	11.0	1	vague	102
-30.75	43.5	10.0	2		93	-44.25	43.0	10.0	2	rvrb	102
-30.75	46.0	10.0	2	2	93	-44.25	47.5	6.0	1	LS.	102
-30.75	61.0	11.5	1	rvrb	93	-44.25	48.0	10.0	3	RHf	102
-30.75	64.0	13.5	1	RHf	93	-44.25	60.0	4.5	2	Г	102
-30.75	71.0	23.0	1	brd_rvrb	93	-44.25	68.5	13.5	1	chevron	102
-30.75	77.5	31.5	1		93	-44.25	74.0	9.0	1	r	102

Easting (ft)	Northing (ft)	2W_TT (ns)	Signal Strength	Comment	Line Number	Easting (ft)	Northing (ft)	2W_TT (ns)	Signal Strength	Comment	Line Number
-44.25	79.0	10.0	1	LHf_brd	102	42.75	64.0	10.0	1	chevron_RHf	107
-44.25	82.5	5.0	3	brd_rvrb	102	42.75	65.0	8.5	2	RHf	107
-44.25	89.0	25.0	1	brd_rvrb	102	42.75	74.0	23.0	1	rvrb	107
-44.25	95.0	6.0	1	r	102	42.75	75.0	9.0	1	symm	107
-44.25	98.0	5.0	2	rvrb	102	44.25	4.5	10.5	1		108
-44.25	102.5	18.0	1	spot	102	44.25	10.0	11.5	2	brd_rvrb	108
-45.75	35.5	7.0	1	flanks	103	44.25	15.0	3.5	3		108
-45.75	47.0	21.5	1	rvrb	103	44.25	18.0	31.0	1	g?	108
-45.75	49.0	12.0	1	spot	103	44.25	21.0	30.5	1	distort	108
-45.75	52.5	13.5	1	brd	103	44.25	50.0	18.0	1	brd_flanks	108
-45.75	63.0	22.0	1	brd_vague	103	44.25	58.0	6.0	3		108
-45.75	72.0	11.0	1	brd_asymm	103	44.25	63.5	5.5	3	brd	108
-45.75	82.0	21.5	1	-	103	44.25	67.0	28.5	- 1	brd_rvrb	108
-45.75	92.0	25.5	1		103	44.25	75.0	8.5	2	symm	108
-45.75	98.0	11.0	1	rvrb	103	44.25	95.0	5.0	3	nnw_rvrb	108
-45.75	102.5	6.5	1	brd	103	44.25	99.0	5.0	3	nnw_rvrb	108
38.25	2.0	24.0	1	brd_rvrb	104	45.75	7.0	32.5	1	111111111111111111111111111111111111111	109
38.25	7.0	6.5	2	brd	104	45.75	12.5	14.5	1	vague	109
38.25	9.0	5.0	3	brd_flanks	104	45.75	20.5	29.5	1	vague	109
38.25	10.5	23.5	1	brd_rvrb	104	45.75	50.0	15.0	3	bed	
38.25		6.0	2	bid_ivib						brd	109
	12.0			had Banka	104	45.75	53.0	7.0	3	rvrb	109
38.25	17.5	7.5	3	brd_flanks	104	45.75	58.0	6.0	3	rvrb	109
38.25	18.5	21.0	1	brd_chevrons	104	45.75	62.5	7.5	2		109
38.25	24.0	6.0	3	brd_flanks	104	45.75	76.5	7.0	2		109
38.25	26.0	32.5	1	doublet	104	45.75	78.0	6.5	2		109
38.25	29.0	6.5	3	brd_rvrb	104	45.75	80.0	5.0	2		109
38.25	32.5	11.0	1		104	45.75	94.0	4.0	3	rvrb	109
38.25	36.0	14.0	2		104	47.25	8.0	5.0	2	brd_rvrb	110
38.25	42.0	31.0	1	brd	104	47.25	10.0	21.5	1	rvrb	110
38.25	42.5	7.5	2	brd	104	47.25	11.0	15.5	1	rvrb	110
38.25	46.0	10.5	3	nrrw_rvrb	104	47.25	22.0	4.5	3	brd	110
38.25	48.5	10.5	3	rvrb_brkn	104	47.25	50.0	14.0	3	brd_rvrb	110
38.25	50.0	29.0	1	brd asymm	104	47.25	60.0	6.0	2	asymm	110
38.25	52.0	21.5	1	RHf	104	47.25	78.0	8.0	3		110
38.25	62.0	11.0	2	nmw_rvrb	104	47.25	93.0	21.5	1	brd_rvrb	110
38.25	70.0	3.5	3		104	47.25	99.5	2.5	3		110
38.25	74.5	11.5	1	rvrb_brkn	104	48.75	6.5	8.0	1	nrrw_rvrb	
38.25	74.5 77.5	8.0	2							chevron	111
				rvrb	104	48.75	10.0	15.0	1	brd	111
38.25	87.5	27.5	1	brd	104	48.75	15.0	16.0	1	vague	111
38.25	98.0	3.0	3	brd_rvrb	104	48.75	20.5	8.0	2	- г	111
39.75	5.0	3.0	3	brd_brkn	105	48.75	42.0	5.5	3	r	111
39.75	8.0	32.5	1	brd_spot	105	48.75	50.0	12.0	1	brd_flanks	111
39.75	9.0	4.5	3	r	105	48.75	83.0	27.5	. 1	brd_vague	111
39.75	12.0	32.5	1	brd_spot	105	48.75	89.5	3.5	3	rvrb	111
39.75	17.5	28.0	1	brd_flattop	105	48.75	92.0	5.5	3	nrw_rvrb	111
39.75	18.5	18.0	1	chevron	105	48.75	94.0	3.0	3	rvrb	111
39.75	20.0	11.5	1	broken	105	50.25	8.0	28.5	1	brd	112
39.75	24.0	11.0	1	brd_LHf	105	50.25	13.5	7.0	1	rvrb	112
39.75	28.0	10.0	2	brd_flanks	105	50.25	17.0	32.0	1	spot	112
39.75	35.5	15.0	2	RHfs	105	50.25	42.5	8.0	3	brd_rvrb	112
39.75	41.0	31.5	1	brd	105	50.25	47.5	3.0	3	r r	112
39.75	41.5	8.0	3	rvrb	105	50.25	49.0	14.0	1	rvrb	112
39.75	46.0	10.0	3	nrrw rvrb	105	50.25	58.0	11.0	1	brd	112
39.75	51.0	29.0	1	brd_rvrb	105	50.25	66.5	12.5	i	brd_RHf	112
39.75	53.0	10.0	2	brd	105	50.25	73.0	12.0	1		112
39.75	57.0	11.5	1	bid	105		85.0		1	spot_vague	
39.75	58.0	19.0			105	50.25		15.5	3	rvrb_vague	112
		A. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	1			50.25	90.0	4.0		uttw_tvtp	112
39.75 39.75	60.5	5.0 20.0	3	rvrb_brkn	105	50.25	94.0	5.0	3	brd	112
	64.0		1	chevrons	105	51.75	16.0	21.5	1	brd_rvrb	113
39.75	67.0	30.0	1	chevron	105	51.75	19.0	10.0	1		113
39.75	72.0	9.5	2	RHf	105	51.75	46.0	10.5	2		113
41.25	4.0	33.0	1	vague	106	51.75	48.0	3.0	3	nnw_rvrb	113
41.25	7.5	15.0	1	brd_RHf	106	51.75	54.0	9.0	1	rvrb	113
41.25	10.0	12.5	. 1	brd_RHf	106	51.75	55.6	12.0	1	RHf	113
41.25	15.0	30.5	1	brd_vague	106	53.25	5.0	9.0	. 1		114
41.25	20.0	33.0	1	brd	106	53.25	7.0	6.0	1	rvrb	114
41.25	23.5	2.0	brd	r	106	53.25	19.0	7.5	1		114
41.25	27.0	30.0	1	brd	106	53.25	23.0	3.5	3	nrw_rvrb	114
41.25	33.0	14.0	2	r	106	53.25	42.5	14.0	- 1	RHf	114
41.25	56.5	11.0	2	brd_LHf	106	53.25	48.0	11.0	i	RHf	114
41.25	60.0	10.5	2	RHf	106	53.25	57.0	6.5	3	brd	114
41.25	72.5	25.5	1	brd_vague	106	53.25	64.0	3.5	3	nrrw_rvrb	114
41.25	77.0	4.0	3	brd_vague brd	106	53.25	81.0	17.5	1	brd_RHf	114
41.25	77.5	23.5	1		106	53.25			1		
				brd_vague			82.5	7.5		spot	114
42.75	2.0	8.0	1	be-	107	53.25	94.5	27.5	1	brd_rvrb	114
42.75	4.0	11.0	1	brd	107	54.75	2.5	26.5	1	nrw_rvrb	115
42.75	8.0	5.0	3	brd	107	54.75	23.5	21.0	1	spot_vague	115
42.75	13.5	7.0	1	r	107	54.75	42.5	13.5	2	asynn	115
42.75	16.5	23.5	1	brd_rvrb	107	54.75	48.0	4.0	3		115
42.75	24.0	11.0	3		107	54.75	79.0	11.0	1	LHf_vague	115
42.75	26.0	11.5	3		107	54.75	88.0	20.5	1	brd_rvrb	115
42.75	27.0	25.5	1	brd_chevrons	107	54.75	95.0	26.0	1	brd	115
42.75	55.0	9.5	2		107	54.75	96.0	3.5	5		115
42.75	60.0	20.0	1	flanks	107	56.25	12.0	26.0	1	brd_RHf	116

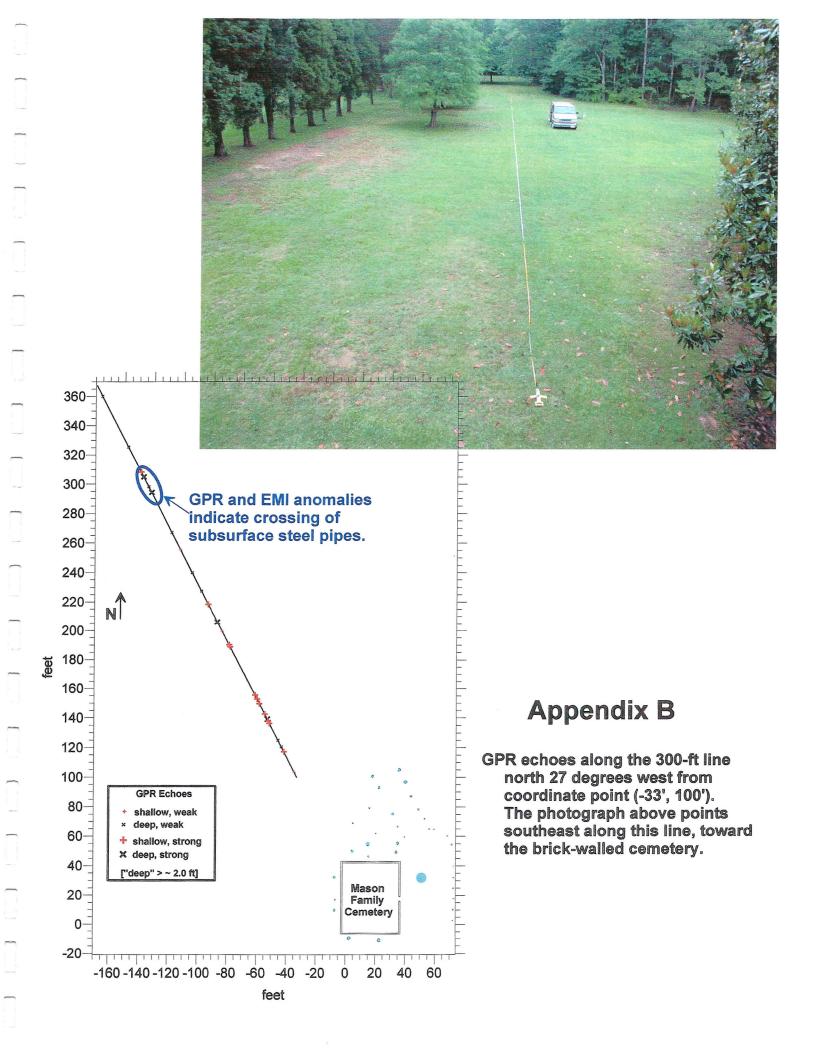
Easting (ft)	Northing (ft)	2W_TT (ns)	Signal Strength	Comment	Line Number	Easting (ft)	Northing (ft)	2W_TT (ns)	Signal Strength	Comment	Line Number
56.25	13.0	11.0	1	brd	116	65.25	65.0	11.5	1	brd	122
56.25	19.0	4.0	3	nrw_rvrb	116	65.25	68.0	16.0	1		122
56.25	23.5	4.0	3	to the second	116	65.25	72.0	16.0	1		122
56.25	43.0	4.0	3	brd_rvrb	116	65.25	74.0	16.5	1		122
56.25	48.5	4.5	3	brd_rvrb	116	65.25	77.5	7.0	1	LHf	122
56.25	53.0	18.5	.1	rvrb	116	65.25	95.0	25.0	1	brd_rvrb	122
56.25	61.5	12.0	3		116	66.75	4.0	6.5	1		123
56.25	73.0	6.5	3	brd_rvrb	116	66.75	10.0	11.0	1	brd	123
56.25	88.0	24.0	1	brd_LHfs	116	66.75	14.5	6.5	1		123
56.25	95.0	25.0	1	brd_rvrb	116	66.75	21.0	7.0	2		123
57.75	9.0	17.0	1	brd_rvrb	117	66.75	22.0	3.5	3	nnw_rvrb	123
57.75	15.0	27.0	1	brd_rvrb	117	66.75	42.0	6.5	3	brd_flanks	123
57.75	18.5	5.0	3	brd	117	66.75	49.0	5.0	3	Did_naino	123
		18.0	1		117	66.75	52.0	13.0	2	flooks	
57.75	20.0			brd_vague						flanks	123
57.75	22.5	5.0	2	brd_rvrb	117	66.75	56.0	13.0	. 1	chevron	123
57.75	25.0	6.5	2	ппж	117	66.75	67.5	7.0	2	brd	123
57.75	27.0	21.0	1	prd_rvrb	117	66.75	80.0	7.0	1	LHf	123
57.75	37.5	5.0	3	brd_rvrb	117	66.75	85.0	7.5	1	RHf	123
57.75	42.0	8.0	2		117	68.25	4.0	6.5	1		124
57.75	47.0	10.5	1		117	68.25	7.5	6.5	1	brd	124
57.75	48.0	19.0	1	chevrons	117	68.25	9.5	6.0	1		124
57.75	52.0	9.0	1		117	68.25	18.0	5.5	1		124
57.75	57.0	10.5	1	rvrb	117	68.25	23.5	5.5	1		124
57.75	76.5	8.0	1	brd flanks	117	68.25	43.0	9.0	3	brd_rvrb	124
57.75	95.0	28.0	i i	brd_rvrb	117	68.25	49.0	4.0	3	510_1115	124
		10.0	1	DIQ_IVID		68.25	52.5	9.0	2	hed nuth	
59.25	2.5				118					brd_rvrb	124
59.25	10.5	6.5	1	brd	118	68.25	68.0	7.5	. 1	brd_RHf	124
59.25	18.0	4.0	3	rvrb	118	68.25	71.0	9.5	1	brd_RHfs	124
59.25	35.0	13.0	1	brd_RHfs	118	68.25	77.5	8.0	1	brd_rvrb	124
59.25	50.0	6.0	2	brd_RHf	118	68.25	81.0	6.0	2		124
59.25	80.0	10.0	1		118	68,25	83.0	6.0	2		124
59.25	86.5	7.5	2		118	68.25	94.0	4.5	3	rvrb	124
60.75	2.0	5.5	2		119	68.25	97.5	4.0	3	rvrb	124
60.75	3.0	20.0	1	brd_rvrb	119	69.75	2.5	5.0	1 .		125
60.75	12.5	32.5	2	dp_clr	119	69.75	6.5	3.5	2		125
60.75	17.5	4.0	3		119	69.75	9.0	9.0	3	brd_RHf	125
60.75	22.5	7.0	1		119	69.75	15.0	23.5	1	brd_rvrb	125
60.75	46.0	5.0	2		119	69.75	17.5	6.0	2	rvrb	125
	48.5	6.0	2		119	69.75	24.0	3.0	3	IVID	125
60.75								8.5	2	n seb	
60.75	52.5	13.5	1	chevron	119	69.75	43.0			rvrb	125
60.75	57.5	9.5	2		119	69.75	49.0	8.0	1	brd_LHf	125
60.75	59.0	9.5	2		119	69.75	69.0	7.0	2		125
60.75	64.0	6.0	2	rvrb	119	69.75	75.0	10.0	1		125
60.75	66.0	10.5	2		119	69.75	93.0	6.0	2	rvrb	125
60.75	74.0	5.5	3	brd	119	69.75	97.5	2.0	rvrb		125
60.75	85.0	23.0	1	brd_rvrb	119	71.25	17.0	7.5	1	brd_chevron	126
60.75	93.0	21.0	1	brd_LHf	119	71.25	24.5	7.5	1	brd_RHf	126
62.25	4.0	26.5	1	vague	120	71.25	43.0	9.0	3	brd_rvrb	126
62.25	8.0	12.0	1	brd	120	71.25	67.0	6.5	1	brd	126
62.25	13.5	10.5	1	rvrb	120	71.25	71.0	7.0	1	chevrons	126
62.25	17.0	6.0	2		120	71.25	78.0	5.0	2	rvrb	126
62.25	19.0	6.5	1	rvrb	120	71.25	98.0	6.0	1	chevrons	126
62.25	21.5	5.5	2		120	72.75	2.0	11.0	1		127
62.25	24.5	7.5	2		120	72.75	6.0	5.0	3		127
62.25	27.5	5.0	3	RHfs	120	72.75	20.0	6.5	1	nrw_rvrb	127
62.25	31.0	7.0	3	rvrb	120	72.75	28.0	10.0	2	1111W_1V1D	127
		9.5	2	brd	120	72.75	30.0	8.5	2		127
62.25	43.5			biu							
62.25	54.0	7.5	2 2 2	20 Lake	120	72.75	36.5	6.0 5.0	3	rvrb	127
62.25	58.0	8.0	2	rvrb	120	72.75	43.0			brd_rvrb	127
62.25	66.5	6.5	2	brd_rvrb	120	72.75	48.0	9.0	1	brd_RHf	127
62.25	77.5	7.0	1		120	72.75	54.0	6.5	2	nnw_rvrb	127
62.25	82.0	27.5	1	brd	120	72.75	62.0	12.5	1	spot	127
62.25	87.0	7.0	2		120	72.75	67.5	11.0	1		127
62.25	92.0	19.5	1	brd_chevrons	120	72.75	75.0	17.0	1	rvrb_chevrons	127
63.75	2.0	4.5	2		121	72.75	95.0	5.0	2	nrrw_rvrb	127
63.75	7.5	14.5	1	rvrb	121	74.25	3.0	4.0	rvrb	r	128
63.75	12.0	29.5	2	dp_clr	121	74.25	13.5	4.5	3	r	128
63.75	41.0	10.0	1	brd_RHf	121	74.25	19.0	4.0	3	nnw_rvrb	128
63.75	47.0	10.0	1	-	121	74.25	25.0	6.0	3	brd_rvrb	128
63.75	49.0	5.5	3		121	74.25	43.0	9.5	2	brd_rvrb	128
	57.0	13.0	1	chevrons	121	74.25	46.5	5.5	2	0.0_1410	128
63.75			1	GIONOIS	121	74.25	53.5	5.0	3		128
63.75	61.0	10.5								bed	
63.75	63.0	6.0	2	brd	121	74.25	57.0	6.0	1	brd_rvrb	128
63.75	67.5	6.0	2	brd	121	74.25	60.5	7.5	1		128
63.75	76.5	7.5	2		121	74.25	62.5	6.5	2	flanks	128
63.75	78.0	8.0	1		121	74.25	73.5	5.0	2	flanks	128
63.75	86.5	7.0	1		121	74.25	76.0	31.0	1		128
63.75	92.0	21.0	1	rvrb_spot	121	74.25	89.0	5.0	2		128
65.25	2.0	4.0	2		122	74.25	99.0	5.0	3	nrrw_rvrb	128
65.25	12.0	27.0	1	brd_rvrb	122	75.75	2.5	6.0	2	rvrb	129
65.25	42.0	10.5	i	brd_RHf	122	75.75	10.5	11.5	1	brd_chevron	129
65.25	49.0	4.5	3		122	75.75	14.0	7.0	1	brd	129
65.25	51.0	4.5	3		122	75.75	25.5	6.0	3	rvrb	129
65.25	55.0	6.0	3		122	75.75	52.0	7.5	2	brd	129
00.20	55.0	0.0	5						-		

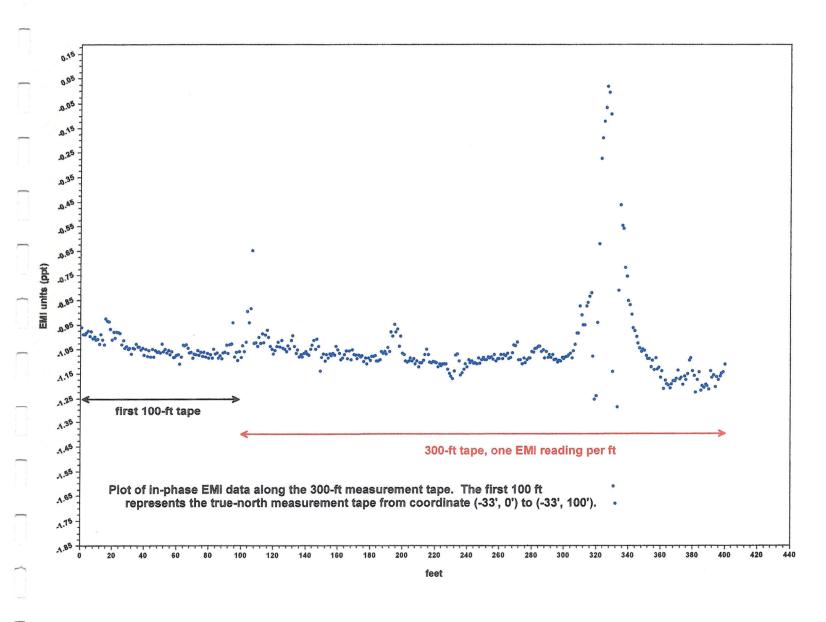
Easting (ft) 75.75	Northing (ft) 53.5	2W_TT (ns) 4.0	Signal Strength	Comment	Line Number 129	Easting (ft) 84.75	Northing (ft) 83.0	2W_TT (ns) 21.5	Signal Strength	Comment	Line Number
75.75	62.0	7.0	3	brd	129	84.75	91.0	6.0	1	brd_rvrb	135 135
75.75	67.5	6.5	2	brd_rvrb	129	86.25	33.5	30.0	1	nnw_rvrb	136
75.75	74.0	5.0	2	rvrb	129	86.25	41.5	5.5	3	brd_flanks	136
75.75	96.0	4.0	3	nmw_rvrb	129	86.25	56.0	9.0	1	nmw_rvrb	136
75.75	97.0	31.5	1	brd_vague	129	86.25	67.0	6.5	1	111147_1415	136
77.25	3.0	4.5	3	z.a_ragao	130	86.25	68.0	6.5	1		136
77.25	8.0	4.5	2		130	86.25	79.0	27.0	1	brd	136
77.25	12.0	4.5	2		130	86.25	84.5	24.0	1	brd_spot	136
77.25	28.0	6.5	2	brd rvrb	130	87.75	27.0	5.0	2		137
77.25	31.5	8.0	1	brd	130	87.75	34.0	6.0	3	rvrb	137
77.25	33.5	6.5	2	brd	130	87.75	42.0	7.5	3	brd_flanks	137
77.25	36.0	6.0	brd	г	130	87.75	52.0	6.0	1	rvrb	137
77.25	41.0	5.5	1	spot	130	87.75	57.5	6.0	1		137
77.25	46.0	7.0	2		130	87.75	68.5	23.0	1		137
77.25	53.0	3.0	2	rvrb	130	87.75	81.0	20.5	1	doublet	137
77.25	55.0	7.0	1		130	36.75	58.5	13.0	1	chevron	138
77.25	67.5	10.0	1	chevron	130	36.75	67.0	10.5	2	flanks	138
77.25	75.0	6.0	1		130	36.75	72.0	8.5	1	chevron_spot	138
77.25	77.0	32.0	1 1		130	36.75	75.0	18.0	2		138
77.25	82.0 88.0	31.5 5.5	2	spot	130	36.75	77.0	27.0	1	rvrb	138
77.25 77.25	89.0	30.0	1	hed nuch	130 130	36.75	83.5 87.5	17.5 30.5	1	chevrons	138
77.25	96.0	5.0	1	brd_rvrb nrrw	130	36.75 36.75	97.0	5.0	1	brd_vague	138
78.75	7.5	7.5	1	flanks	131	35.25	59.0	8.0	2 1	nrw_rvrb	138 139
78.75	57.5	8.5	i	rvrb	131	35.25	72.0	6.0	2	uuw_tvtp	139
78.75	60.0	5.0	2	1410	131	35.25	78.5	29.0	1	vague	139
78.75	62.5	5.0	2		131	35.25	92.5	15.0	i	rvrb_brkn	139
78.75	65.0	4.5	2		131	35.25	97.0	7.0	2	nrw_rvrb	139
78.75	75.0	31.0	1	brd	131	33.75	57.0	17.0	1	brd_RHf	140
78.75	90.0	30.0	1	brd_rvrb	131	33.75	58.0	4.0	3	rvrb	140
78.75	95.5	32.0	1	_	131	33.75	77.0	13.5	1	rvrb_brkn	140
80.25	2.0	4.0	2		132	33.75	82.0	18.0	1	chevron_LHf	140
80.25	2.5	5.5	1	chevrons	132	32.25	59.0	10.5	3	nrrw	141
80.25	3.0	22.0	1	brd_vague	132	32.25	62.0	16.0	1	RHf_brkn	141
80.25	6.5	5.0	2		132	32.25	65.0	18.5	1		141
80.25	10.5	5.5	2	RHf	132	32.25	67.5	16.0	1	brd	141
80.25	47.0	7.0	3		132	32.25	97.5	6.0	3	r	141
80.25	52.0	5.0	2	rvrb	132	30.75	57.0	8.0	3		142
80.25	62.5	5.0	2	rvrb	132	30.75	58.0	21.0	1	chevron	142
80.25	66.0	4.0	2	r.	132	30.75	60.0	10.0	2		142
80.25	74.0	7.5 30.0	1	rvrb	132	30.75	65.0	17.0	1	brd	142
80.25	77.0 88.5	32.0	1	brd	132	30.75	66.0 68.5	5.0	3 1	<u>r</u>	142
80.25 81.75	2.0	5.0	2	brd_vague	132 133	30.75 30.75	82.5	24.0 8.0	1	nпw	142
81.75	6.0	5.0	2		133	30.75	97.0	15.5	1	RHfs	142 142
81.75	10.5	5.0	2		133	30.75	100.0	16.5	1	RHfs	142
81.75	13.5	7.5	1	chevrons	133	30.75	103.0	24.0	1	brd	142
81.75	20.0	29.0	1	brd_rvrb	133	29.25	47.5	10.5	3	rvrb	143
81.75	22.0	18.0	1	brd_vague	133	29.25	48.0	13.0	2	RHf	143
81.75	55.5	5.0	2		133	29.25	52.5	10.0	2	rvrb	143
81.75	60.0	6.5	2		133	29.25	55.0	10.0	2		143
81.75	66.0	6.0	2		133	29.25	60.0	9.0	3		143
81.75	78.0	10.0	1	distort	133	29.25	62.0	7.5	2	rvrb	143
81.75	80.5	20.0	1	prd_rvrb	133	29.25	68.0	12.0	1		143
83.25	27.5	7.0	2		134	29.25	77.0	11.0	2	nrrw	143
83.25	28.5	7.0	2	01	134	29.25	78.0	6.5	2	rvrb	143
83.25	34.0	5.0 7.5	3 2	flanks	134	29.25	79.0	12.0	]	g/r?	143
83.25 83.25	38.0 56.5	21.5	1	r	134 134	29.25 29.25	81.5 95.0	7.5 7.0	1 1	rvrb RHfs	143
83.25	60.0	8.0	1	RHf	134	29.25	98.0	10.0	1	brd_chevrons	143 143
83.25	64.0	4.0	2	KIII	134	27.75	48.0	10.5	2	brd_spot	144
83.25	66.5	4.0	3	RHf	134	27.75	54.5	10.0	2	rvrp	144
83.25	70.0	28.0	1	brd_chevron	134	27.75	60.0	11.0	2	IVID	144
83.25	73.0	11.0	1	spot	134	27.75	69.5	10.0	1		144
83.25	76.0	32.0	i	spot	134	27.75	71.0	14.0	1		144
83.25	97.0	32.0	i	opot	134	27.75	76.5	5.5	3		144
83.25	98.0	21.0	1	LHf	134	27.75	78.0	12.0	1		144
84.75	22.0	8.0	1	rvrb	135	27.75	98.0	10.0	2	brd	144
84.75	25.0	5.0	1		135	26.25	48.0	8.0	3	brd_brkn	145
84.75	27.5	8.0	3	brd	135	26.25	54.0	7.5	2	rvrb	145
84.75	33.5	5.5	2		135	26.25	60.0	7.5	3	nested	145
84.75	34.0	5.5	2		135	26.25	64.0	10.0	1	rvrb	145
84.75	38.0	7.0	2		135	26.25	67.0	17.0	1	chevrons	145
84.75	41.5	6.0	3	brd_RHf	135	26.25	72.5	11.5	2	brd_brkn	145
84.75	44.5	5.0	2		135	26.25	76.0	5.0	3	nrrw_rvrb	145
84.75	45.0	30.0	1	brd_rvrb	135	26.25	80.0	11.0	1		145
84.75	48.0	7.5	1		135	26.25	98.0	18.0	1	brd	145
84.75	52.0	6.0	1		135	24.75	46.0	10.5	2	r?	146
84.75	57.5	24.0	1	brd	135	24.75	48.0	10.0	3	r?	146
84.75	64.0	5.5	1	chevron	135	24.75	51.5	9.5	1 3	chevron	146
84.75 84.75	67.5 74.0	7.0 <b>4.0</b>	1 2	chevron	135 135	24.75 24.75	53.0 60.5	10.0 16.0	1	rvrb brd RHf	146 146
84.75	77.5	17.0	1		135	24.75	62.5	25.0	1	brd_RHf rvrb	146
J 1 U					.50	24.70	02.0	20.0			

Easting (ft)	Northing (ft)	2W_TT (ns)	Signal Strength	Comment	Line Number	Easting (ft)	Northing (ft)	2W_TT (ns)	Signal Strength	Comment	Line Number
24.75	66.0	17.0	2	brd_rvrb	146	11.25	74.0	17.0	1	flanks	156
24.75	72.0	12.0	1	rvrb	146	11.25	76.0	14.0	1		156
24.75	78.0	10.5	1	nnw	146	11.25	88.0	6.0	2		156
24.75	90.0	10.0	1	brd	146	11.25	92.0	11.0	2		156
24.75	94.0	6.0	2	nrrw	146	11.25	95.0	11.0	1	rvrb	156
24.75	102.0	28.0	1	brd_rvrb	146	11.25	98.0	12.0	2	rvrb	156
23.25	47.0	8.0	2	uuw_tvtp	147	11.25	102.0	10.5	1	r	156
23.25	53.0	7.5	3	brd_spot	147	11.25	104.0	10.0	1	Γ	156
23.25	64.0	7.0	3	nrw	147	9.75	48.0	26.0	1		157
23.25	67.5	13.0	2	brd_rvrb	147	9.75	52.0	10.0	2		157
23.25	76.0	12.0	1	RHf	147	9.75	57.0	18.0	2	rvrb	157
23.25	92.0	31.0	1	brd_rvrb	147	9.75	59.0	11.0	1		157
23.25	100.5	5.0	3	nnw_rvrb	147	9.75	62.5	6.0	2		157
23.25	104.5	11.0	2	LHfs	147	9.75	67.0	16.0	1	chevron_spot	157
21.75	52.0	13.5	2	rvrb	148	9.75	69.5	7.0	1	rvrb	157
21.75	65.5	18.5	1	brd	148	9.75	80.0	31.0	1		157
21.75	67.0	8.0	1	nnw	148	9.75	86.5	31.0	1		157
21.75	68.5	9.5	1	rvrb -	148	9.75	90.0	11.0	2	rvrb	157
21.75	72.0	11.0	. 1	brd_spot	148	9.75	95.0	8.5	3		157
21.75	78.0	13.0	1	rvrb	148	9.75	97.0	9.0	2		157
21.75	101.0	6.0	3		148	8.25	48.0	6.5	2		158
20.25	47.5	11.0	2	brd	149	8.25	52.5	11.0	2	rvrb	158
20.25	51.5	7.5	2	1?	149	8.25	59.0	11.0	2		158
20.25	52.0	13.0	1	brd	149	8.25	62.5	6.5	2	brd_rvrb	158
20.25	55.0	16.5	1	spot	149	8.25	72.0	13.5	1	rvrb_vague	158
20.25	63.5	10.0	1		149	8.25	77.5	6.0	3	brd_brkn	158
20.25	66.5	18.0	1	spot	149	8.25	82.0	27.0	1	brd_rvrb	158
20.25	67.0	6.5	1	chevron	149	8.25	87.5	28.0	1	brd_rvrb	158
20.25	69.5	14.5	2		149	8.25	94.0	10.0	2	_	158
20.25	70.0	14.5	2	g?	149	8.25	99.0	12.5	1	RHf	158
20.25	75.5	13.5	2	3.	149	8.25	101.0	10.0	2		158
20.25	77.0	12.0	2		149	6.75	63.0	12.0	2	brd_rvrb	159
20.25	81.0	10.0	1		149	6.75	66.0	14.0	1		159
20.25	92.5	13.0	2	brd rvrb	149	6.75	74.0	26.0	1	RHf	159
		6.5	3	DIG_IVID	149	6.75	83.0	7.5	3	brd_rvrb	159
20.25	101.0	10.0	3	hed nuth	150	6.75	89.0	28.0	1	chevrons	159
18.75	47.5		3	brd_rvrb	150	6.75	100.0	29.0	1	brd_rvrb	159
18.75	51.0	9.0	1	rvrb	150	6.75	104.0	14.0	2	LAUP.	159
18.75	62.0	9.0 9.0	2	brd_rvrb	150	5.25	62.5	10.0	3	rvrb	160
18.75	67.5		2	rvrb		5.25	64.0	4.0	2	nnw_rvrb	160
18.75	70.0	15.0	1	g/r	150 150	5.25	68.0	4.0	2	IIIIW_IVID	160
18.75	77.5	21.0		rvrb			84.0	10.0	2	brkn	160
18.75	89.0	7.0	2	nrrw_rvrb	150	5.25	86.0	9.0	2	DIKII	160
18.75	91.5	11.0	2	brd	150	5.25	99.0	24.0	1	rvrb	160
18.75	93.5	12.5	1		150	5.25	47.5	13.0	1	rvrb	161
18.75	97.0	24.0	1	vague	150	3.75			1		
17.25	61.0	11.5	1	RHf	152	3.75	50.0	19.5		brd_rvrb	161
17.25	67.5	11.0	3	rvrb	152	3.75	52.5	10.0	2	n.m.	161
17.25	69.5	15.5	3	rvrb	152	3.75	57.0	12.0	2	rvrb	161
17.25	72.0	15.0	2	rvrb	152	3.75	59.0	11.0	2	nrrw_chevrons	161
17.25	79.0	10.5	1	brd_rvrb	152	3.75	62.0	7.0	2	nrw_rvrb	161
17.25	83.5	24.0	1	brd_rvrb	152	3.75	67.0	11.0	2	rvrb	161
17.25	89.0	6.0	3	nrw_rvrb	152	3.75	69.0	16.0	1	rvrb	161
15.75	60.5	14.0	2	2	153	3.75	71.5	11.5	2	rvrb	161
15.75	68.0	11.0	3	brd_rvrb	153	3.75	79.0	10.0	2	rvrb	161
15.75	69.0	16.0	1	brd	153	3.75	82.0	7.0	2		161
15.75	72.5	17.0	1	chevron	153	3.75	87.0	27.0	1	brd_rvrb	161
15.75	79.0	10.0	2	rvrb	153	3.75	93.0	28.0	1	brd_rvrb	161
15.75	82.0	27.0	1	prd_rvrb	153	3.75	97.0	8.0	1		161
15.75	87.0	11.0	2		153	2.25	49.0	8.0	2	rvrb	162
15.75	96.0	22.0	1	rvrb	153	2.25	53.0	15.0	1	vague	162
15.75	98.0	16.0	1	RHfs	153	2.25	56.0	13.0	1	ппw	162
15.75	101.0	7.0	2	chevrons	153	2.25	57.5	8.0	2	chevrons	162
14.25	62.0	12.5	2	brd_rvrb	154	2.25	67.0	12.5	1		162
14.25	65.5	6.0	2	nrrw_rvrb	154	2.25	71.5	9.0	3	rvrb	162
14.25	69.0	10.5	3	brd_rvrb	154	2.25	74.0	6.5	1		162
14.25	72.0	11.0	3	brd_rvrb	154	2.25	79.0	10.0	3	rvrb	162
14.25	81.5	18.0	1	RHfs	154	2.25	82.0	10.0	1		162
14.25	87.5	5.0	3	nrrw_rvrb	154	2.25	97.5	6.0	2		162
14.25	99.0	8.5	2	rvrb	154	2.25	100.0	11.0	2		162
14.25	102.5	10.0	1	chevrons	154	0.75	54.0	11.5	1	nrrw_rvrb	163
12.75	65.0	29.0	1	brd_rvrb	155	0.75	56.5	11.0	3		163
12.75	71.0	8.0	1	100000 🛥 100.70 🖂	155	0.75	58.5	8.5	1		163
12.75	72.0	10.0	3	rvrb	155	0.75	61.0	6.5	3	nrrw_rvrb	163
12.75	75.0	11.0	3	rvrb	155	0.75	65.5	28.0	1	brd_rvrb	163
12.75	80.5	18.5	1	brd	155	0.75	75.0	13.5	1	LHfs	163
		25.0	1	brd_rvrb	155	0.75	79.0	11.0	2		163
12.75	87.5		3	DIG_IVID	155	0.75	82.0	6.0	2		163
12.75	92.5	10.0	2	rvrb	155	-0.75	57.0	11.0	3		164
12.75	98.5	8.0		LFf	155	-0.75	60.0	7.5	1		164
12.75	101.0	11.0	1	r?	155	-0.75	64.0	13.0	i	brd	164
12.75	104.0	7.0	2	r? nrrw_chevrons	156	-0.75 -0.75	65.0	28.0	1	brd_rvrb	164
11.25	46.0	9.0	1		156	-0.75	74.0	29.0	1	brd_chevrons	164
11.25	52.5	10.0	3	rvrb RHfs	156	-0.75 -0.75	79.0	10.5	2	DIG_CHEVIONS	164
11.25	55.0	17.0	1	RHfs	156	-0.75	98.5	25.0	3	dp_metall	164
11.25	62.0	12.0	2	rvrb	100	-0.75	30.0	20.0	U	ap_inotali	.04

## Appendix A: GPR Echoes, Mason Family Cemetery area

Easting (ft)	Northing (ft)	2W_TT (ns)	Signal Strength	Comment	Line Number
-2.25	52.5	11.5	1		165
-2.25	62.5	18.0	1	vague	165
-2.25	67.0	32.0	1	brd	165
-2.25	74.0	18.0	1		165
-2.25	77.0	12.0	1		165
-2.25	79.5	10.0	1		165
-2.25	89.0	31.5	. 1		165
-2.25	100.0	26.0	3	brd_metall	165
-2.25	104.0	7.5	2	rvrb	165





## APPENDIX C

What our experience has taught us about detecting old graves

In general, a grave site can be geophysically detected *directly* or *indirectly*. It can be detected *directly* by sensing the buried human remains, objects buried with the remains, or the burial container. It can be detected *indirectly* by sensing the soil characteristics of backfill in the grave shaft. Both *direct* and *indirect* detection of grave sites by GPR often involves sensing groups of reflectors that are just as likely to be located at the edges of the grave as at the center of the grave. We have discovered elsewhere that gravestones can be mis-placed by several feet relative to the burial, that gravestones and fieldstones mark only a small percentage of burials in some old cemeteries, and that burials, including burial containers, can be reduced to mere silhouettes or shadows in the subsurface. As expected, graves of children or infants are usually much more difficult to detect than graves of adults because of their smaller size. Also, as expected, of two extremes, it is most difficult to detect a shroud burial and easiest to detect a metallic-coffin burial.

Direct detection of grave sites may involve the sensing of more massive bones, such as the skull, femur, and tibia; coffin hardware (handles, finials, knobs, escutcheons, glass viewing panes); objects attached to the interred (jewelry and favorite possessions), and knotty sections of pine boxes, which are much more resistant to decomposition than other woody parts. The cloth of shroud burials occasionally escapes decomposition, especially if it has been in contact with a brass or copper-based metal object—button, pendant, or buckle--, which protects it from bacterial decay. Environmental factors detrimental to preservation include extremely acidic or extremely alkalic soil and poor drainage resulting in alternating wet-dry subsuface conditions.

Indirect detection of grave sites may involve the sensing of disturbed soil in the grave shaft (a chaotic GPR pattern as compared to a stratified pattern or a sharp GPR lateral discontinuity representing the side of the grave shaft) and objects contained in the backfill, such as rocks or metallic items.

Not unexpectedly, we have discovered that *direct* detection of early and mid-19th-century graves in the Piedmont usually is difficult (compared to late-19th-century graves and those more recent), regardless of methods used, because of dissolution of the buried remains, attached objects, and burial containers, if any. *Indirect* detection also is more difficult because the older the grave, the more compacted the soil surrounding the burial, and the less contrast of disturbed soil relative to undisturbed soil. Preservation conditions are usually much better in the Atlantic Coastal Plain where Gunston Hall Plantation resides.

The most effective ways to delineate these old graves are

(1) by using a steel probe with custom-made bulbous tip, supplemented by using a spoon-tipped coring tool, in the hands of an experienced archaeologist or soil scientist in order to ascertain whether or not the soil is disturbed--as it must be if it is part of a grave shaft. This probing is

sometimes difficult or impossible to accomplish if the soil is frozen, dry-hardened, or exceptionally stony.

(2) by stripping the topsoil in order to visually detect the presence and exact location of a grave shaft on the basis of contrasts in soil color and texture.

It is prudent beforehand or concurrently to use remote-sensing techniques, such as GPR, to help establish where to probe and where to excavate the topsoil. The interred remains themselves often are reduced to "shadows", merely a fraction of an inch thick.

In general, we find that most 19th-century burials are surprisingly shallow--often less than half of the traditionally assumed 6-ft depth. Fortunately, even in adverse soil conditions, it is not necessary for the radar energy to penetrate much below the topsoil in order to detect some characteristics of the grave-shaft soil. It also is our experience that graves sometimes can be detected by reflections from subsurface tree roots and groundhog burrows that invade old grave shafts, following the path of least resistance.

Users of GPR data should recognize that neither this technique nor any other remote-sensing technique can *unambiguously* detect the presence of very old graves in normal circumstances. It is important to remember that GPR signals associated with *a single grave* can be shallow and/or deep; can be weak and/or strong; and can emanate from any part of the grave--from center to edges or top to bottom of the grave shaft.

## Dimensions of graves

Today, the average size of a modern casket for adult burial is 84 inches long, 28 inches wide, and 23 inches high. A medium-size grave liner (an unsealed receptacle into which the casket is optionally placed) is 86 inches by 30 inches by 24 inches. A medium size burial vault (a sealed receptacle into which the casket is optionally placed) is 86 inches by 29 inches by 25 inches. Although receptacles may be larger or much smaller (for children), the dimensions of most caskets, liners, and vaults are similar. The rectangular (in plan view) grave shaft, usually dug by use of a backhoe but dug by hand where backhoe access is denied, must be a few inches greater in length and width than the largest container emplaced. These rectangular dimensions also approximately apply to the hexagonal toe-pincher coffins commonly used in the 18th, 19th and early 20th centuries.